# Pavement Deterioration Modeling Using Historical Roughness Data 

by

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A Thesis Presented in Partial Fulfillment of the Requirements for the Degree Master of Science

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## ARIZONA STATE UNIVERSITY

May 2016


#### Abstract

Pavement management systems and performance prediction modeling tools are essential for maintaining an efficient and cost effective roadway network. One indicator of pavement performance is the International Roughness Index (IRI), which is a measure of ride quality and also impacts road safety. Many transportation agencies use IRI to allocate annual maintenance and rehabilitation strategies to their road network.

The objective of the work in this study was to develop a methodology to evaluate and predict pavement roughness over the pavement service life. Unlike previous studies, a unique aspect of this work was the use of non-linear mathematical function, sigmoidal growth function, to model the IRI data and provide agencies with the information needed for decision making in asset management and funding allocation. The analysis included data from two major databases (case studies): Long Term Pavement Performance (LTPP) and the Minnesota Department of Transportation MnROAD research program. Each case study analyzed periodic IRI measurements, which were used to develop the sigmoidal models.

The analysis aimed to demonstrate several concepts; that the LTPP and MnROAD roughness data could be represented using the sigmoidal growth function, that periodic IRI measurements collected for road sections with similar characteristics could be processed to develop an IRI curve representing the pavement deterioration for this group, and that pavement deterioration using historical IRI data can provide insight on traffic loading, material, and climate effects. The results of the two case studies concluded that in general, pavement sections without drainage systems, narrower lanes, higher traffic, or measured


in the outermost lane were observed to have more rapid deterioration trends than their counterparts.

Overall, this study demonstrated that the sigmoidal growth function is a viable option for roughness deterioration modeling. This research not only to demonstrated how historical roughness can be modeled, but also how the same framework could be applied to other measures of pavement performance which deteriorate in a similar manner, including distress severity, present serviceability rating, and friction loss. These sigmoidal models are regarded to provide better understanding of particular pavement network deterioration, which in turn can provide value in asset management and resource allocation planning.

## DEDICATION

This thesis is dedicated to my parents, family, and friends whose continual support has helped me throughout my education and during the development of this research work. I am grateful for their unconditional love, compassion, and understanding.

## ACKNOWLEDGMENTS

The author would first like to express utmost gratitude to her advisor, Professor Kamil E. Kaloush, who provided invaluable instruction, support, encouragement, and guidance from the beginning of the author's graduate program at Arizona State University. His support and guidance aided in the development of the author's interest in pavement engineering, this research topic, and the success in her graduate studies. Deepest gratitude is also due to the members of the supervisory committee, Professor Shane Underwood and Professor Michael Mamlouk, who provided instruction, guidance, and support throughout the author's graduate program and this research work.

This research was supported in part by Arizona State University funding, through a research assistantship that allowed the author to pursue her area of interest. The author is deeply appreciative for the support of the National Center of Excellence (NCE) for SMART Innovations and ASU's University Transportation Center (UTC). The author also would like to acknowledge the Long-Term Pavement Performance program (LTPP) and the Minnesota Road Research Project (MnROAD), for making available and providing the necessary data for this research.

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## DEFINITIONS

| AADT | Annual Average Daily Traffic |
| :--- | :--- |
| AADTT | Annual Average Daily Truck Traffic |
| AC | Asphalt Concrete |
| ASTM | American Society for Testing and Materials |
| ESAL | Equivalent Single Axel Load |
| LISA | Lightweight Inertial Surface Analyzer |
| LTPP | Mong Term Pavement Performance |
| MnDOT | Minnesota Department of Transportation |
| MnROAD | Mechanistic-Empirical Pavement Design Guide |
| MEPDG | Pavement Condition Index |
| PCI | Partland Cement Concrete |
| PCC | Present Serviceability Rating |
| PMS | Strategic Highway Research Program |
| PSR | MHRP |

## 1. INTRODUCTION

### 1.1 Background

### 1.1.1. Pavement Management Systems

The primary goals of pavement management systems (PMS) are to maintain or improve the quality of the roadway network, while utilizing available funding in the most effective and beneficial way. Pavement management systems not only prioritize the maintenance of already deteriorated roadway segments, but also utilize historic data and deterioration modelling to plan for future conditions. There is a significant benefit to preventative pavement maintenance; as minor maintenance treatments on pavements still in good condition have a higher cost-effectiveness than major rehabilitation of a deteriorated pavement. The use of pavement management systems allows the optimum use of available resources (e.g., money and materials) while meeting set constraints of budget and time requirements (Molenaar, 2001). Pavement management systems can be used at the local, county, state, or federal level. Benchmarking and tracking the condition changes within the roadway network are important in predicting future deterioration and managing assets.

### 1.1.2 Pavement Roughness

Pavement roughness values are measured in the form of an international roughness index (IRI), which is a primary indication of ride quality. The IRI was developed in 1982 as part of an international experiment conducted in Brazil. It constitutes the smoothness, safety, and the ease of the driving path (Prasad et al., 2013). The IRI depends on the pavement distresses present, it is a measure of the surface texture, and it is a key indicator in driving safety. The IRI is usually correlated to roughness measurements obtained from both response-type and inertial-based profiler systems (Sayers 1990). The international
roughness index is measured in units of slope, and it describes the suspension motion of a moving vehicle over a travelled distance, usually in meters per kilometer or inches per mile (Park et al., 2007). The IRI ranges from $0 \mathrm{~m} / \mathrm{km}$ to $20 \mathrm{~m} / \mathrm{km}$ (greatest roughness). The Federal Highway Administration (FHWA) provided guidelines on the various IRI measures as shown in the Table 1 below (FHWA 1999). IRI is also calculated in accordance with ASTM Standard E 1926 (ASTM 1999e).

Table 1: IRI and Condition (FHWA, 1999)

| Condition <br> Categories | PSR Rating |  | IRI Rating, $\mathbf{m} / \mathbf{k m}(\mathbf{i n} / \mathbf{m i})$ |  | Interstate and NHS <br> Ride Quality |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Interstate | Other | Interstate | Other |  |
| Very Good | $\geq 4.0$ | $\geq 4.0$ | $<1.0(<60)$ | $<1.0(<60)$ | Acs <br> Good |
| Goss than Acceptable |  |  |  |  |  |
| Fair | $3.5-3.9$ | $3.5-3.9$ | $1.0-1.5(60-94)$ | $1.0-1.5(60-94)$ | $>2.0(>170)$ |
| Mediocre | $2.6-3.0$ | $2.6-3.4$ | $1.5-1.9(95-119)$ | $1.5-2.0(95-170)$ |  |
| Poor | $\leq 2.5$ | $\leq 2.0$ | $1.9-2.0(120-170)$ | $2.0-3.5(171-220)$ | $>2.0(>170)$ |

Notes: PSR $=$ Present serviceability rating, NHS $=$ National Highway System.

Pavements with high IRI values can be indicative of surface distresses, uneven pavement, and low ride quality. Higher IRI values are more accepted in low volume rural areas than in high volume highways. In pavement management, surface distresses and roughness are measured periodically in order to set benchmark values and predict future conditions.

### 1.1.3 Sigmoidal Function

Pavement performance is dependent on traffic loading, climatic conditions, material selection, and structural composition. The general shape of the pavement performance function (loss of serviceability) is classically described as an " S " shaped curve. This deterioration pattern in pavements has been acknowledged by many researchers, including

Riggins et al. (1984) and Sotil and Kaloush (2004). The pavement performance deterioration concept is shown in Figure 1.


Figure 1: Pavement Performance Function, Sigmoidal "S" Shaped Curve

This concept applies to many aspects of pavement condition, including the Pavement Condition Index (PCI) and Present Serviceability Rating (PSR). These measures of pavement condition begin at a high level (desirable) and worsen to a low level over time. This trend is represented mathematically as a sigmoidal function and can take different shape forms.

The sigmodal function was selected due to its previous successful application in pavement condition modeling; it also best represents the pavement deterioration process. A similar pattern is expected in pavement roughness deterioration, except that decay is traded by growth. At the beginning of a pavement's life, the measured roughness values are low with excellent ride quality. Noticeable deterioration is not common over the first several years of pavement life. After the first few years, small distresses begin to form, which start to
affect the roughness minimally. Once these distresses become apparent, the pavement begins more to deteriorate more rapidly. The deterioration slows after a certain level is reached. This trend follows the shape of the sigmoidal growth curve.

### 1.2 Research Objectives

The objective of the analysis in this study was to develop a methodology to evaluate and predict pavement roughness over the pavement service life. Based on historical roughness data collected, a local, county, or state agency can develop a model to predict how the pavement surface will deteriorate over time. The ability to plan for future pavement deterioration allows the jurisdiction to develop a maintenance strategy timeline.

### 1.3 Proposed Concept

A sigmoidal growth model to be evaluated and constructed to simulate the roughness deterioration pattern in pavements. The proposed roughness sigmoidal model is the inverse of the classic pavement performance function; the desired pavement roughness is initially low but increases over time. The analysis aims to demonstrate the following concepts:

- LTPP IRI data can be represented using a sigmoidal growth function
- IRI measurements collected for road sections with similar characteristics could be processed to develop a fitted "family" sigmoidal curve representing pavement deterioration for this group.
- Pavements separated further into subgroups can provide meaningful results which compare deterioration patterns between similar groups
- Pavement subgroups with the following characteristics will deteriorate more rapidly than their counterparts:
- High traffic loading sections (compared to low traffic conditions)
- Freezing climate sections (compared to more moderate climates)
- Primary driving lane (outer) sections (compared to inner or passing lane)
- Standard lane-width sections compared to some wider lane-width designs
- Sections with and without adequate drainage systems

A graphical representation of the proposed concepts is shown in Figure 2.


Figure 2: Proposed Deterioration between Pavement Subgroups

### 1.4 Scope of Research

The analysis in this study used data from the Long Term Pavement Performance (LTPP) InfoPave database and the Minnesota Road Research Program (MnROAD). To develop the methodology for predicting pavement roughness, pavement sections from Arizona (LTPP) and Minnesota (MnROAD Test Track) were used as case studies. The historical roughness (IRI) data (measured on a frequent basis, approximately once every 6-18 months) of each pavement section was analyzed to develop sigmoidal models representing deterioration. These models can then be used to predict pavement roughness over the service life if there is no planning for future maintenance action. The goal was to determine the IRI over time, demonstrate the time until the IRI reaches an unacceptable level. The process developed in this analysis can be useful for pavement management and applied to other performance measures.

### 1.5 Organization of Thesis

In the next chapter, a literature review outlines the concepts and theories related to pavement condition management and modeling. Past research efforts which identify current conditions and develop models to predict future pavement conditions are discussed. In Chapter 3, the methodology of this research is provided, which includes a discussion of the data sources and formats, data processing, and the conceptual framework for developing the IRI sigmoidal master curves. This process of developing sigmoidal curves is demonstrated in Chapters 4 and 5, which use historical data collected over the past 25 years from pavement test sections in Arizona and Minnesota. Chapter 4 is a case study using Arizona roadway sections from the LTPP InfoPave database, and Chapter 5 is a case study using Minnesota roadway sections provided from MnDOT's pavement test track,

MnROAD. The concepts, methods, and results are concluded in Chapter 6, which also provides additional recommendations for the implementation of this research into practice.

## 2. LITERATURE REVIEW

### 2.1 Pavement Management Purpose

There are three primary objectives of a pavement management system: to implement more cost-effective treatment strategies, allocate funding to the pavement sections that will result in the best performance, and improve the quality of the pavement network (AASHTO, 2001). The goal of a pavement management system is to allocate funding in the most beneficial way towards the roadway network. The planning and scheduling of maintenance is crucial in preserving pavement condition; preventative maintenance extends the service life of a pavement and delays the need for serious rehabilitation or reconstruction. Pavement maintenance strategies can be used at either the project level, focusing on a small selection of pavement, or network level, which considers many pavement sections within an area (Haas, Hudson, \& Zaniewski, 1994). The processes and methodology developed in this research is designed as a network level pavement management tool. The basic components of a network level PMS are shown in Figure 3 (FHWA, 1995).


Figure 3: Network Level PMS Components

This research study will add value to the "Condition Assessment", as future prediction will be available in addition to existing conditions. This information will better help to prioritize maintenance efforts using available funding.

### 2.2 IRI Measurement Process

The development of roughness testing began in the 1970's and 1980's with funding by the World Bank and the National Cooperative Highway Research Program (Park et al., 2007). The World Bank originally funded research to determine cost effective maintenance techniques, and it was discovered that roughness was a main source of user costs derived from poor pavement surfaces. The American Society for Testing and Materials (ASTM) has developed standard testing methods for pavement roughness using a profilograph. The testing device is a "platform comprised of dollies articulated by rigid members or trusses so that all the wheels are supporting the profilograph" (ASTM, 2012). The profilograph consists of 12 wheels, has a minimum length of 23 ft , and obtains roughness measurements as it moves longitudinally across the pavement section.

More recently, there are several other common roughness measuring devices which include response-type measuring systems (Maysmeter and Roadmeter) and other inertial road profiling systems (Profiler and Profilometer) (Kaloush, 2014). Profile-measuring vehicles are most commonly utilized than truss profilographs due to the ease of use and consistency. Rather than manually translating the profilograph, an operator can measure pavement roughness simply by driving along the pavement. ASTM has also developed standards for this method of data collection, referred to as an "Accelerometer Established Inertial Profiling Reference". This method continually measures elevation variation of the pavement surface as it moves longitudinally along the pavement (ASTM, 2009). Inertial
profiling systems are able to cover a large pavement network and process data electronically. The IRI datasets included in this research work were measured using inertial profiling systems.

### 2.3 Pavement Condition Deterioration in Pavement Groups

Pavement performance and the rate of deterioration depend on many factors; the layer structure and materials, quality of construction, intensity of traffic loading, and the climatic conditions.

Construction variability has a significant impact on long term pavement performance (Sebaaly \& Bazi, 2004). Extensive planning goes into material selection and mix design, however poor construction practices, such as uneven mixing or insufficient compaction can reduce the long term performance.

Traffic is the primarily responsible for problems associated with pavement performance (Pais, Amorim, \& Minhoto, 2013). More specifically, the performance is impacted by load intensity, frequency, and axle and tire configuration. Heavy traffic causes fatigue cracking and rutting, both of which increase the IRI measurement. Trucks are of primary concern, as they carry much greater weight and axle loads. Pavement damage increases rapidly as axle loads increase. A study performed by the City of Fort Collins, Colorado, attempted to evaluate the impacts of routine garbage trucks on residential streets. This study concluded that the pavement damage caused by vehicles increases at a higher than proportional rate as vehicle size and weight increase (R3 Consulting Group, Inc., 2008). Heavier traffic loads are expected to cause more pavement deterioration than lower traffic loads.

Temperature and precipitation also affect pavement performance. The presence of freezing temperatures can cause pavement problems, including thermal, fatigue and frost related
cracking, pavement rutting (due to thaw), potholes, and crack deterioration (Zubeck \& Dore, 2009). Excess moisture that is not able to sufficiently drain from the pavement structure can also cause damage, even if it remains in the subgrade.

### 2.4 IRI Modeling Approaches

Previous studies were reviewed to develop and support methodology used in this study. Included in this review is an IRI prediction model based on the pavement properties, distresses, and external factors; and IRI backcasting model, used to linearly interpolate missing IRI data; and lastly, a sigmoidal pavement performance model representing pavement condition index (PCI) changes over time.

### 2.4.1 The World Bank HDM-IV Model

Pavement roughness prediction models typically predict the IRI at a certain time using a baseline IRI, the time elapsed since the baseline, pavement thickness, traffic loading, environmental factors, and pavement distress observations. The World Bank HDM-IV flexible pavement smoothness model predicts IRI using a combination of distress, environmental, traffic, structural, and material factors. The developed World Band HDMIV Model (Watanatada, 1987, M-E PDG, 2001):

Equation 1: World Bank HDM - IV Model

$$
\begin{aligned}
\Delta R I= & 134 e^{m t} M S N K^{-5.0} \Delta N E 4+0.114 \Delta R D S=0.0066 \Delta C R X+0.003 h \Delta P A T+ \\
& 0.16 \Delta P O T+m R I_{t} \Delta t
\end{aligned}
$$

Where:
$\Delta R I \quad=$ increase in roughness period over time period $\Delta t$
$M S N K \quad=$ a factor related to pavement thickness, structural number and cracking
$\triangle N E 4 \quad=$ incremental number of equivalent standard-axle loads (ESALs) in period
$\Delta t \quad=$ change in time
$\triangle R D S \quad=$ increase in rut depth, mm
$\triangle C R X \quad=$ percent increase in area of cracking

| $\triangle P A T$ | $=$ percent increase in surface cracking |
| :--- | :--- |
| $\triangle P O T$ | $=$ increase in total volume of potholes, $\mathrm{m}^{3} / l \mathrm{lane} \mathrm{km}$ |
| $m$ | $=$ environmental factor |
| $R I_{t}$ | $=$ roughness at time t, years |
| $\Delta t$ | $=$ incremental time period for analysis, years |
| $t$ | $=$ average age of pavement or overlay, years |
| $h$ | $=$ average deviation of patch from original pavement profile, mm |

This method incorporates many factors and can account for daily and hourly variation in temperature, moisture, and traffic.

### 2.4.2 MEPDG IRI Backcasting Method

In the Mechanical-Empirical Pavement Design Guide (M-E PDG), linear modelling is expressed as a practical method in determining the initial IRI in sections which data collection began after the roadway section was opened to traffic. This method was a backcasting technique used to fill missing LTPP IRI data (M-E PDG, 2001). The basis of the model was:

Equation 2: IRI Backcasting Model
$I R I=f(a g e)$
The initial IRI was found by determining the location of the $y$-intercept of the straight line which was fit to the known points. This technique has weaknesses; however, as it was determined that the backcasted initial IRI values were significantly different than the measured initial IRI.

### 2.4.3 Pavement Condition Index Deterioration Superposition Model

In the previous research by Sotil and Kaloush (2004), a sigmoidal decay model was developed to predict the pavement condition index (PCI) over time. The sigmoidal function developed is as follows:

## Equation 3: PCI Sigmoidal Model

$P C I=a+\frac{b}{1+E X P(c \cdot T+d)}$
Where:
PCI = Condition as dependent variable
$T \quad=$ Reduced (shifted) time as independent variable
$a \quad=$ Constant representing minimum PCI value
$a+b=$ Constant representing maximum PCI value
$c, d \quad=$ Parameters describing the shape of the sigmoidal function

The research described the process of developing the sigmoidal curve using the superposition of sections. This model allowed for the future PCI to be predicted in the absence of future maintenance activities. Each roadway section was evaluated, a decrease in PCI from one year to the next was found (evidence of maintenance), the segment was broken into two, both starting at time $(t)=0$. Each of the broken segments were used in the model, and they were individually shifted by a time factor to move to the appropriate lateral location on the sigmoidal curve. The sigmoidal curve was fit to best represent the data. This model was developed as a tool to benefit the pavement management of a roadway network and the prioritization of maintenance activity.

The sigmoidal curve and time shifting methodology discussed above was further developed and modified in this research to reflect pavement roughness deterioration.

## 3. METHODOLOGY

### 3.1 Process

The methodology described in this section utilizes historical pavement roughness data, typically collected from a local, regional, or state transportation agency. The measured roughness data is collected regularly using consistent calibrated equipment and standardized techniques. A sufficient timespan of data, reflecting pavement performance over time, is necessary to develop a performance curve, and pavements of varying age should be considered. Ideally, the modeling process would include roadway sections which were regularly measured over 25 years, from the time the roadway was open to traffic. In practical applications this is not always possible. In these cases, it is important to capture a sufficient quantity of roadway sections in various phases of the deterioration or performance curve. For example, developing a reliable model of lifetime pavement deterioration is not possible if only data of road sections of one to five years in age are considered.

This modeling approach produces a prediction tool for pavement roughness conditions if no further maintenance or reconstructed efforts are implemented. In addition, the constructed performance curve only considers the deterioration on roadway sections in between maintenance intervention. The process separates the complete timespan of collected IRI data on a roadway segment into multiple series. For example, if maintenance occurred at year $5,8,12$, and 15 , there are five separate series for modeling (years $0-5$, years $5-8$, years $8-12$, years $12-15$, and years $15+$ ). If maintenance has not been adequately documented within the data, maintenance can be generally identified by a significant drop in IRI between two dates of collected measurements.

The best source of historical data for the modeling effort is from routine profilometers measurements. The data should be stored in a database which also documents material, construction, drainage, traffic, maintenance, and climatic (based on roadway network size) information. This additional information is used to create several specific models for parts of the roadway network with similar characteristics, which provides more accurate prediction. Asphalt Concrete (AC) and Portland Cement Concrete (PCC) sections should have distinct predictive models, as the timeline and process in which they deteriorate is different. In a large network of diverse roadway sections, a more accurate prediction for a particular roadway segment will come from a performance model that is built with sections of the same subgroup (i.e., sections with similar traffic levels or sections within the same climatic region).

A group of hypothetical roadway sections will be used to demonstrate the modeling process used in this methodology chapter. This example will extend through the other subsections within Chapter 3. The "measured" IRI data of the hypothetical five roadway sections of similar characteristics are presented in Table 2, which represent data throughout the service life of a typical pavement section. For example, Roadway Section 1 includes data from 1987 to 2006 and includes 20 IRI measurements (on average, one measurement every 12 months). The other 4 roadway sections include data which span different time periods.

Table 2: Data Demonstration - IRI Measurements of Five Roadway Segments

| Roadway Section | Date of Measurement | Measured IRI (m/km) | Roadway Section | Date of Measurement | Measured IRI (m/km) | Roadway Section | Date of Measurement | Measured IRI (m/km) | Roadway Section | Date of Measurement | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Date of Measurement | Measured IRI (m/km) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 11/11/1987 | 1.00 | 2 | 5/2/2001 | 3.00 | 3.00 | 9/13/1999 | 3.50 | 4 | 8/9/1993 | 2.50 | 5 | 10/31/1974 | 2.10 |
|  | 9/9/1988 | 1.10 |  | 8/7/2001 | 3.20 |  | 10/4/2001 | 3.50 |  | 3/27/1995 | 2.70 |  | 5/29/1975 | 2.30 |
|  | 5/24/1989 | 1.10 |  | 12/4/2002 | 3.40 |  | 2/11/2003 | 3.60 |  | 10/10/1995 | 2.80 |  | 6/28/1976 | 2.80 |
|  | 1/16/1990 | 1.20 |  | 7/7/2003 | 3.70 |  | 4/3/2003 | 3.65 |  | 4/2/1996 | 2.90 |  | 1/31/1977 | 3.00 |
|  | 6/27/1990 | 1.20 |  | 3/15/2004 | 2.00 |  | 6/10/2003 | 3.70 |  | 8/13/1996 | 3.00 |  | 7/1/1977 | 3.40 |
|  | 2/5/1992 | 1.30 |  | 8/9/2004 | 2.10 |  | 10/30/2003 | 3.70 |  | 8/31/1998 | 3.10 |  | 10/21/1977 | 3.70 |
|  | 11/10/1993 | 1.50 |  | 3/9/2005 | 2.20 |  | 7/6/2004 | 3.80 |  | 2/29/2000 | 3.30 |  | 12/14/1977 | 4.00 |
|  | 3/17/1995 | 1.80 |  | 4/26/2005 | 2.40 |  | 1/17/2005 | 3.80 |  | 10/25/2000 | 3.70 |  | 7/6/1978 | 1.00 |
|  | 7/21/1995 | 2.00 |  | 1/2/2006 | 2.60 |  | 1/27/2005 | 3.90 |  | 6/22/2001 | 3.90 |  | 8/24/1978 | 1.00 |
|  | 12/12/1995 | 2.40 |  | 4/6/2007 | 3.20 |  | 6/1/2006 | 4.00 |  | 11/22/2001 | 4.10 |  | 3/30/1979 | 1.00 |
|  | 2/23/1996 | 0.90 |  | 7/23/2007 | 3.50 |  | 3/20/2007 | 2.50 |  | 12/24/2001 | 1.00 |  | 2/4/1980 | 1.20 |
|  | 9/13/1996 | 1.00 |  | 9/12/2008 | 3.70 |  | 10/2/2007 | 2.70 |  | 4/22/2002 | 1.02 |  | 10/15/1980 | 1.30 |
|  | 7/10/1998 | 1.20 |  | 12/24/2009 | 3.80 |  | 10/2/2008 | 2.90 |  | 7/24/2002 | 1.05 |  | 3/18/1981 | 1.40 |
|  | 5/17/1999 | 1.25 |  | 1/20/2010 | 1.50 |  | 9/11/2009 | 3.10 |  | 8/5/2003 | 1.05 |  | 10/2/1981 | 1.45 |
|  | 3/9/2000 | 1.30 |  | 12/14/2011 | 1.60 |  | 12/17/2009 | 3.50 |  | 7/7/2004 | 1.06 |  | 11/16/1981 | 1.45 |
|  | 11/24/2000 | 1.40 |  | 8/13/2012 | 1.60 |  | 9/9/2011 | 3.60 |  | 3/7/2005 | 1.07 |  | 1/15/1982 | 1.60 |
|  | 3/22/2002 | 1.60 |  | 12/5/2013 | 1.70 |  | 12/27/2011 | 1.50 |  | 11/10/2005 | 1.10 |  | 11/3/1982 | 2.00 |
|  | 9/14/2004 | 1.80 |  | 1/17/2014 | 1.80 |  | 9/19/2012 | 1.50 |  |  |  |  | 12/22/1982 | 0.75 |
|  | 5/2/2005 | 2.20 |  | 4/10/2014 | 1.90 |  | 3/25/2013 | 1.60 |  |  |  |  | 6/6/1984 | 0.80 |
|  | 4/18/2006 | 2.40 |  | 4/14/2014 | 2.00 |  | 4/3/2013 | 1.60 |  |  |  |  | 7/27/1984 | 0.85 |
|  |  |  |  | 9/29/2014 | 2.40 |  | 11/13/2013 | 1.70 |  |  |  |  | 1/23/1985 | 0.85 |
|  |  |  |  | 2/5/2015 | 2.60 |  | 3/23/2014 | 1.70 |  |  |  |  | 7/21/1987 | 0.90 |
|  |  |  |  | 8/4/2015 | 2.90 |  | 10/27/2014 | 1.80 |  |  |  |  | 2/15/1988 | 1.00 |
|  |  |  |  |  |  |  | 1/12/2015 | 1.90 |  |  |  |  | 8/19/1988 | 1.10 |
|  |  |  |  |  |  |  | 6/23/2015 | 1.90 |  |  |  |  | 1/2/1989 | 1.12 |
|  |  |  |  |  |  |  | 10/6/2015 | 2.00 |  |  |  |  | 7/24/1989 | 1.15 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 4/3/1991 | 1.20 |

Figure 4 visually describes this data; each section begins and ends at a unique location. In practical applications, the information of a roadway section may be limited. For example, if there is only a small series of IRI data known for a particular roadway segment but the open-to-traffic date is unknown, it is difficult to determine the appropriate location on the lifetime performance curve. The methodology described in this section utilizes a time shifting process to shift series of IRI measurements to their appropriate location on the performance curve.


Figure 4: Data Demonstration - IRI Measurements of Five Roadway Segments

### 3.2 Data Preparation

The next step in the data preparation process is to standardize the time scale, which allows the measurements of roadway sections of various time periods to be analyzed together. In this step, all roadway segments are modified to begin at "Time $=0$ ". All subsequent time measurements are indicated in units of years. If the first measurement was on 11/11/1987 and the second measurement was on $9 / 9 / 1998$, this converts to Time $=0$ and Time $=0.83$, respectively. The five roadway sections with standardized time is shown in Table 3. This is displayed graphically in Figure 5, where all roadway segments are set to begin at "Time $=0 \prime$.

Table 3: Data Demonstration - IRI Measurements using Standardized Time

| Roadway Section | Standardized Time (Years) | Measured IRI (m/km) | Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.00 | 1.00 | 2 | 0.00 | 3.00 | 3 | 0.00 | 3.50 | 4 | 0.00 | 2.50 | 5 | 0.00 | 2.10 |
|  | 0.83 | 1.10 |  | 0.27 | 3.20 |  | 2.06 | 3.50 |  | 1.63 | 2.70 |  | 0.58 | 2.30 |
|  | 1.53 | 1.10 |  | 1.59 | 3.40 |  | 3.42 | 3.60 |  | 2.17 | 2.80 |  | 1.66 | 2.80 |
|  | 2.18 | 1.20 |  | 2.18 | 3.70 |  | 3.56 | 3.65 |  | 2.65 | 2.90 |  | 2.25 | 3.00 |
|  | 2.63 | 1.20 |  | 2.87 | 2.00 |  | 3.74 | 3.70 |  | 3.01 | 3.00 |  | 2.67 | 3.40 |
|  | 4.24 | 1.30 |  | 3.27 | 2.10 |  | 4.13 | 3.70 |  | 5.06 | 3.10 |  | 2.98 | 3.70 |
|  | 6.00 | 1.50 |  | 3.85 | 2.20 |  | 4.82 | 3.80 |  | 6.56 | 3.30 |  | 3.12 | 4.00 |
|  | 7.35 | 1.80 |  | 3.99 | 2.40 |  | 5.35 | 3.80 |  | 7.22 | 3.70 |  | 3.68 | 1.00 |
|  | 7.70 | 2.00 |  | 4.67 | 2.60 |  | 5.38 | 3.90 |  | 7.87 | 3.90 |  | 3.82 | 1.00 |
|  | 8.09 | 2.40 |  | 5.93 | 3.20 |  | 6.72 | 4.00 |  | 8.29 | 4.10 |  | 4.41 | 1.00 |
|  | 8.29 | 0.90 |  | 6.23 | 3.50 |  | 7.52 | 2.50 |  | 8.38 | 1.00 |  | 5.27 | 1.20 |
|  | 8.85 | 1.00 |  | 7.37 | 3.70 |  | 8.06 | 2.70 |  | 8.71 | 1.02 |  | 5.96 | 1.30 |
|  | 10.67 | 1.20 |  | 8.65 | 3.80 |  | 9.06 | 2.90 |  | 8.96 | 1.05 |  | 6.38 | 1.40 |
|  | 11.52 | 1.25 |  | 8.73 | 1.50 |  | 10.00 | 3.10 |  | 9.99 | 1.05 |  | 6.93 | 1.45 |
|  | 12.33 | 1.30 |  | 10.62 | 1.60 |  | 10.27 | 3.50 |  | 10.92 | 1.06 |  | 7.05 | 1.45 |
|  | 13.05 | 1.40 |  | 11.29 | 1.60 |  | 12.00 | 3.60 |  | 11.58 | 1.07 |  | 7.21 | 1.60 |
|  | 14.37 | 1.60 |  | 12.60 | 1.70 |  | 12.30 | 1.50 |  | 12.26 | 1.10 |  | 8.01 | 2.00 |
|  | 16.85 | 1.80 |  | 12.72 | 1.80 |  | 13.03 | 1.50 |  |  |  |  | 8.15 | 0.75 |
|  | 17.48 | 2.20 |  | 12.95 | 1.90 |  | 13.54 | 1.60 |  |  |  |  | 9.61 | 0.80 |
|  | 18.45 | 2.40 |  | 12.96 | 2.00 |  | 13.56 | 1.60 |  |  |  |  | 9.75 | 0.85 |
|  |  |  |  | 13.42 | 2.40 |  | 14.18 | 1.70 |  |  |  |  | 10.24 | 0.85 |
|  |  |  |  | 13.77 | 2.60 |  | 14.53 | 1.70 |  |  |  |  | 12.73 | 0.90 |
|  |  |  |  | 14.27 | 2.90 |  | 15.13 | 1.80 |  |  |  |  | 13.30 | 1.00 |
|  |  |  |  |  |  |  | 15.34 | 1.90 |  |  |  |  | 13.81 | 1.10 |
|  |  |  |  |  |  |  | 15.79 | 1.90 |  |  |  |  | 14.18 | 1.12 |
|  |  |  |  |  |  |  | 16.07 | 2.00 |  |  |  |  | 14.74 | 1.15 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 16.43 | 1.20 |



Figure 5: Data Demonstration - IRI Measurements using Standardized Time
The IRI data, provided in Table 3 and Figure 5, depicts periods of roughness increase followed by a significant decrease in IRI. This pattern describes regular pavement maintenance performed to extend the service life, which can include pothole patching, crack sealing, and overlays. In this stage of the process the datasets are still in the "raw"
format, as it includes maintenance efforts. The objective is to develop a model that describes how a pavement section would deteriorate in the absence of any maintenance intervention. This is accomplished by studying the deterioration patterns in between maintenance efforts, and superimposing these smaller sections to understand the lifetime behavior. In Table 3, red bars separate the IRI data of each roadway section into smaller series. These locations are identified by a significant decrease in IRI between two periodic measurements, which indicate maintenance activity between the two readings. These smaller subsections are separated in Table 4, and are hereafter referred to as "series".

Table 4: Data Demonstration - IRI Measurements using Standardized Time, Separated by Maintenance Efforts

| Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Standardized Time (Years) | Measured IRI (m/km) | Roadway Section | Standardized <br> Time (Years) | Measured IRI (m/km) | Roadway Section | Standardized Time (Years) | Measured IRI ( $\mathrm{m} / \mathrm{km}$ ) | Roadway Section | Standardized Time (Years) | Measured IRI (m/km) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1A | 0.00 | 1.00 | 2A | 0.00 | 3.00 | 3A | 0.00 | 3.50 | 4A | 0.00 | 2.50 | 5A | 0.00 | 2.10 |
|  | 0.83 | 1.10 |  | 0.27 | 3.20 |  | 2.06 | 3.50 |  | 1.63 | 2.70 |  | 0.58 | 2.30 |
|  | 1.53 | 1.10 |  | 1.59 | 3.40 |  | 3.42 | 3.60 |  | 2.17 | 2.80 |  | 1.66 | 2.80 |
|  | 2.18 | 1.20 |  | 2.18 | 3.70 |  | 3.56 | 3.65 |  | 2.65 | 2.90 |  | 2.25 | 3.00 |
|  | 2.63 | 1.20 | 2B | 0.00 | 2.00 |  | 3.74 | 3.70 |  | 3.01 | 3.00 |  | 2.67 | 3.40 |
|  | 4.24 | 1.30 |  | 0.40 | 2.10 |  | 4.13 | 3.70 |  | 5.06 | 3.10 |  | 2.98 | 3.70 |
|  | 6.00 | 1.50 |  | 0.98 | 2.20 |  | 4.82 | 3.80 |  | 6.56 | 3.30 |  | 3.12 | 4.00 |
|  | 7.35 | 1.80 |  | 1.12 | 2.40 |  | 5.35 | 3.80 |  | 7.22 | 3.70 | 5B | 0.00 | 1.00 |
|  | 7.70 | 2.00 |  | 1.80 | 2.60 |  | 5.38 | 3.90 |  | 7.87 | 3.90 |  | 0.13 | 1.00 |
|  | 8.09 | 2.40 |  | 3.06 | 3.20 |  | 6.72 | 4.00 |  | 8.29 | 4.10 |  | 0.73 | 1.00 |
| 1B | 0.00 | 0.90 |  | 3.36 | 3.50 | 3B | 0.00 | 2.50 | 4B | 0.00 | 1.00 |  | 1.58 | 1.20 |
|  | 0.56 | 1.00 |  | 4.50 | 3.70 |  | 0.54 | 2.70 |  | 0.33 | 1.02 |  | 2.28 | 1.30 |
|  | 2.38 | 1.20 |  | 5.78 | 3.80 |  | 1.54 | 2.90 |  | 0.58 | 1.05 |  | 2.70 | 1.40 |
|  | 3.23 | 1.25 | 2 C | 0.00 | 1.50 |  | 2.48 | 3.10 |  | 1.61 | 1.05 |  | 3.24 | 1.45 |
|  | 4.04 | 1.30 |  | 1.90 | 1.60 |  | 2.75 | 3.50 |  | 2.54 | 1.06 |  | 3.37 | 1.45 |
|  | 4.76 | 1.40 |  | 2.56 | 1.60 |  | 4.48 | 3.60 |  | 3.20 | 1.07 |  | 3.53 | 1.60 |
|  | 6.08 | 1.60 |  | 3.88 | 1.70 | 3 C | 0.00 | 1.50 |  | 3.88 | 1.10 |  | 4.33 | 2.00 |
|  | 8.56 | 1.80 |  | 3.99 | 1.80 |  | 0.73 | 1.50 |  |  |  | 5C | 0.00 | 0.75 |
|  | 9.19 | 2.20 |  | 4.22 | 1.90 |  | 1.24 | 1.60 |  |  |  |  | 0.73 | 0.80 |
|  | 10.16 | 2.40 |  | 4.23 | 2.00 |  | 1.27 | 1.60 |  |  |  |  | 1.58 | 0.85 |
|  |  |  |  | 4.69 | 2.40 |  | 1.88 | 1.70 |  |  |  |  | 2.28 | 0.85 |
|  |  |  |  | 5.05 | 2.60 |  | 2.24 | 1.70 |  |  |  |  | 2.70 | 0.90 |
|  |  |  |  | 5.54 | 2.90 |  | 2.84 | 1.80 |  |  |  |  | 3.24 | 1.00 |
|  |  |  |  |  |  |  | 3.05 | 1.90 |  |  |  |  | 3.37 | 1.10 |
|  |  |  |  |  |  |  | 3.49 | 1.90 |  |  |  |  | 3.53 | 1.12 |
|  |  |  |  |  |  |  | 3.78 | 2.00 |  |  |  |  | 4.33 | 1.15 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 4.47 | 1.20 |

For example, there is evidence of two individual maintenance efforts within the Roadway Segment 2 dataset. The significant decreases in IRI (maintenance efforts) are shown in Figure 6 in the shaded regions. Based on the maintenance efforts, Roadway Section 2 is separated into three series. In order to standardize the time scale and analyze each series as a separate piece of data, each new series is also shifted to begin at "Time $=0$ ".


Figure 6: Data Demonstration - Roadway Section 2 Maintenance Efforts

Figure 7 shows the separated series within Roadway Section 2 shifted to begin at "Time $=$ $0 "$. This process is continued for the other four roadway sections, and their separated series are shown together in Figure 8.


Figure 7: Data Demonstration - Roadway Section 2 Separated Series


Figure 8: Data Demonstration - Pavement Performance, Separating Maintenance Efforts

Each IRI data series must be in the standardized time format, shown in Table 4 and Figure 8, to continue with the next step of the methodology.

### 3.3 Development of Performance Curves

### 3.3.1 Sigmoidal Function

Similar to the PCI sigmoidal decay function (Equation 3), the appropriate Sigmoidal Growth Function used in this research effort is shown below (Equation 4). Essentially, the difference is in the negative coefficient $a_{3}$ which reverses the shape of the classical sigmoidal function.

Equation 4: Sigmoidal Growth Function
$I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$

Where:

$$
\begin{aligned}
& I R I=\text { International Roughness Index }(\mathrm{m} / \mathrm{km}) \\
& a_{1}=\text { Lower IRI Limit } \\
& \left.a_{2}=\text { Factor affecting the IRI Upper Limit (Upper IRI Limit }=a_{1}+a_{2}\right) \\
& a_{3}=\text { Factor affecting the rate of deterioration } \\
& a_{4}=\text { Factor affecting the start time and rate of deterioration } \\
& t=\text { Offset Time (Years) }
\end{aligned}
$$

### 3.3.2 Excel Solver Optimization

The parameters, $a_{1}, a_{2}, a_{3}$, and $a_{4}$, were used to develop a unique sigmoidal function based on the group of separated series. Excel Solver was used to individually shift each series and minimize the difference between the series location and the best-fit sigmoidal curve.

To facilitate the sigmoidal parameter fitting in Excel Solver, several parameter constraints were used. The parameter constraints are shown in Table 5. Based on the sigmoidal growth function selected for the analysis, all four parameters $\left(a_{1}, a_{2}, a_{3}\right.$, and $\left.a_{4}\right)$ are required to be positive. Another constraint was placed on parameter $\mathrm{a}_{2}$, which affects the upper IRI limit. The upper IRI limit in the model is the sum of parameters $a_{1}$ and $a_{2}$. Although true pavement roughness deterioration does not have an absolute limit, a maximum value was selected for consistency across the various simulated models. A maximum value $\left(a_{1}+a_{2}\right)$ of IRI was assumed to be between 4 and 5 meters per kilometer. The most roughness data is available when the offset time ( t ) is zero, and it was observed that many of the sections began at an IRI between 0.5 and 1.0 meters per kilometer $\left(a_{1}\right)$. Therefore, the $a_{2}$ parameter was constrained to be less than or equal to 3.5 meters per kilometer.

Table 5: Parameters used in Sigmoidal Model Fitting

| Parameter | Constraints Used |
| :---: | :---: |
| a 1 | $\geq 0$ |
| a 2 | $\geq 0, \leq 3.5$ |
| a 3 | $\geq 0$ |
| a 4 | $\geq 0$ |

The Excel spreadsheet template used to develop each sigmoidal curve is provided in Figure 9. This specific spreadsheet was used to determine the sigmoidal curve for the data demonstration of the five roadway sections explained in this chapter. The data for each series (as shown in Table 4) is inputted directly into Columns A-D, which is shown in orange and green blocks. Due to constraints in excel, each series must be equal to or less than 10 measurements (also referred to as data points) If any series is greater than 10 data points, the additional data is added to the subsequent block. This additional "series" can
have the same "ROAD No.", but must begin at "Time $=0$ ". Columns K-N essentially compress the data. Each row within these columns refers to a separate series. It details the IRI of the first data point of the series, and the appropriate lateral time shift (optimized by Excel). Column G explains the "Error", or difference, in the location of the fitted curve and each individual data series. Excel Solver is set to minimize the sum of errors (P1) by changing the model parameters (P2:P5) and the individual shift factor of each series (L2:L14).


Figure 9: Excel Optimization Spreadsheet

This process finds the best sigmoidal curve to fit the data within a set maximum time shift. Several iterations of maximum time shift are conducted to determine the optimal maximum time shift, which is a related to the rate of deterioration and the length of a pavement's service life. Generally, pavement section groups with greater optimal maximum time shifts (i.e., $30-35$ ) are more ideal than those with lower time shifts (i.e., $10-15$ years). If the optimal fit is reached in a short time shift, it indicates that poor condition is reached in a
short period of time. Longer optimal time shifts indicate that the poor condition sections occur later in the pavement's lifetime.

Figures 9,10 , and 11, explain the time shifting process for the hypothetical roadway sections explained in this section. Figure 10 allows for a maximum time shift of only 5 years. This first curve is not the best fit, as some of the sections with high IRI ( $3-4 \mathrm{~m} / \mathrm{km}$ ), could still benefit from a greater time shift.


Figure 10: Data Demonstration - Sigmoidal Fit using a 5 Year Maximum Time Shift

Figure 11 shows the same data, but this time with a maximum time shift of 10 years. With the additional allowable shift time, the individual series are able to shift more closely to the fitted curve.


Figure 11: Data Demonstration - Sigmoidal Fit using a 10 Year Maximum Time Shift

Figure 12 shows the next iteration, with a maximum time shift of 15 years. In this methodology, providing a greater allowable time shift will always result in a model with a better fit, until a threshold value is reached.


Figure 12: Data Demonstration - Sigmoidal Fit using a 15 Year Maximum Time Shift

### 3.3.3 Model Accuracy and Fit

The optimal allowable time shift for each data group is determined as the time shift iterations reach the threshold value for model accuracy. The relative accuracy ration (Se/Sy) and the coefficient of determination, $R^{2}$ were used as statistical measures of the goodness of fit between the master curve and the shifted segments. Se being the standard error of estimate, Sy being the standard deviation. Se/Sy values are good if less than 0.5 ; and marginal if greater than 0.75 . The $R^{2}$ value can be used if computed based on the $\mathrm{Se} / \mathrm{Sy}$ ratio as follows (Equation 5):

Equation 5: Coefficient of Determination
$R^{2}=1-\left(\frac{n-v}{n-1}\right) *[S e / S y]^{2}$
Where:

$$
\begin{aligned}
& \mathrm{n}=\text { Number of samples } \\
& v=\text { Number of regression coefficients }
\end{aligned}
$$

As the maximum time shift increased, the segments had the ability to shift to a more optimal position, and the $\mathrm{Se} / \mathrm{Sy}$ and $R^{2}$ improved. The maximum time shift is incrementally increased to reach the best fit. The optimal time shift is determined after $R^{2}$ and $\mathrm{Se} / \mathrm{Sy}$ reach a threshold value and no longer significantly increase. This threshold is the smallest incremental increase of $R^{2}$ between two time shift curves that results in essentially the same goodness of fit. This incremental increase threshold for $R^{2}$ must be consistent while developing models for a dataset; for example, a roadway network of either local or statewide, where the data was collected using the same process, equipment, and frequency. This threshold values should only be modified if analyzing two unique datasets; for example, two statewide agencies data with different data collection processes, equipment, and frequency. The modified model sensitivity value may be a better fit for analyzing the comparison of curves of the second network based on the data collection characteristics. Using this technique, it is valuable to compare the optimal time shift curves of pavement groups within a dataset, but not valuable to comparing the time shift of groups in different datasets (i.e., states). The optimal time shift is an indicator of the service life of the pavement, and how quickly it deteriorates to a poor quality.

In this example, it is assumed that the optimal time shift is reached if the next time shift results in $R^{2}$ value that is less than or equal to 0.005 greater than the previous $R^{2}$ value. This assumption is based on previous modeling efforts of historical data. The three time shift curves developed as part of the hypothetical data modeling are shown in Figure 13, with the optimal time shift of 10 years shown in green.


Figure 13: Data Demonstration - Time Shift Curves
An optimal time shift of 10 years was determined by evaluating the measures of fit for each time shift curve. The incremental increase in the $R^{2}$ value from the 10 year shift to the 15 year shift is less than or equal to $0.005(0.0041)$, which indicates that the 10 year shift is the optimal time shift. After the optimal time shift is determined, there is no benefit in analyzing additional time shift periods, which is why only the 5,10 , and 15 year time shifts are analyzed in this hypothetical example. In other data groups, it is necessary to continue to 45 years to reach the threshold value of less than 0.005 in model fit.

Table 6: Data Demonstration - Time Shift Model Coefficients and Measures of Fit

| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.862 | a1 | 0.987 | a1 | 1.008 |
| a2 | 2.811 | a2 | 2.959 | a2 | 2.903 |
| a3 | 0.645 | a3 | 0.545 | a3 | 0.5 |
| a4 | -3.61 | a4 | -4.952 | a4 | -5.876 |
| Se/Sy | 0.4788 | Se/Sy | 0.2044 | Se/Sy | 0.1807 |
| R2 | 0.8941 | R2 | 0.9816 | R2 | 0.9856 |

## 4. CASE STUDY 1: LTPP PAVEMENT ROUGHNESS DATA

### 4.1 Introduction

The Long Term Pavement Performance (LTPP) InfoPave Database was developed as a part of the Strategic Highway Research Program (SHRP) in 1987. The database was created as a system to document pavement attributes, conditions, maintenance activities, and reconstruction efforts over a period of time. Each roadway included in the database has a unique section number, which identifies the location, roadway classification, and material and structure thickness properties. The database will routinely document indicators of pavement performance deterioration, including distresses and roughness, and monitor the conditions over the life of each pavement section.

There are a total of 2509 sections available in the InfoPave database which are located within the United States and Canada. There are five primary categories of information available for each pavement section; these can be used to filter the data and extract only pavement information of interest.

In the General data, the pavement age, experiment type, study group, section name, monitoring status, location, roadway classification, and maintenance and rehabilitation efforts and are identified. The Structure data lists the material types for the surface, base, and subgrade layers. In this category, Asphalt Concrete (AC) and Portland Cement Concrete (PCC) sections can be separated. The Climatic data allows the user to separate pavement sections into the following climate regions: Dry/Freeze, Dry/Non-Freeze, Wet/Freeze, Wet/Non-Freeze. This section also records the annual freezing index, precipitation, and temperature which is experienced by the pavement section. The Traffic data records the annual average daily traffic (AADT) and the annual average daily truck
traffic (AADTT). The final grouping of data are the Performance measures. The deflection, cracking, faulting, and roughness are regularly observed and recorded.

The InfoPave database is useful in conducting pavement performance research. Pavement experiments were conducted to determine the various effects that structure, materials, traffic, climate, and maintenance have on the pavement condition over time.

### 4.2 Data Summary

In the LTPP InfoPave Database there are a total of 146 roadway sections in Arizona; 95 of which are "Asphalt Concrete Pavement" sections. These sections are to be referred to in this document as "asphalt" sections, or more simply, "AC" sections. The roadway sections in the LTPP database are primarily highways and interstates, as a majority of the data collection has been in partnership with state transportation agencies. Local roads are not included in the database. Some roadway sections began data collection at the time it was opened to traffic, while other section studies began after a roadway segment was in operation.

The Arizona roadway sections in the LTPP InfoPave database are within one of two climatic regions: Dry, Non-Freeze or Dry, Freeze. Traffic loading is reported annually in several forms in the LTPP database; however, the traffic data used in this analysis is in the form of equivalent single axle loads (ESALs or represented as KESAL for 1000 units). The Arizona data ranges from 300-4,450 KESALs.

The roughness data is reported in meters per kilometer $(\mathrm{m} / \mathrm{km})$. These measurements were recorded using profilometers, vehicles equipped with sensors to detect the longitudinal profile variation of the pavement. The measurements were collected regularly (approximately once every 6-18 months) over the period of 5-20 years. The roughness data
was measured in two locations, on the left and right wheel paths. This method of measurement is to best replicate the ride quality of the travelling public.

The LTPP data also specifies the type and frequency of maintenance activity. The maintenance actions are referred to as a new "construction number" $(\mathrm{CN})$ in the database. For example, new pavement sections begin as CN 1, and after a chip seal the section becomes a CN 2. The CN increases with each maintenance activity and continues over the entire duration that data is collected for the section. The maintenance information is important, as the analysis aims to standardize the data to model roughness deterioration without the effects of maintenance. The construction number is used to distinguish between phases of each section. Within each phase, or CN , there are no effects of maintenance. These phases are used to create individual, standardized datasets for modeling.

The IRI data of the asphalt sections was separated into subgroups based on the climatic region and intensity of traffic loading. The goal of the analysis is to demonstrate the sigmoidal curve methodology, and additionally to show that deterioration trends can be observed when comparing multiple related pavement characteristic groups. The modeling process of analyzing and constructing sigmoidal curves was conducted for the following pavement section groups in Table 7.

Table 7: LTPP Data Grouping Summary

| Data <br> Source | Comparison | Name | Number of <br> Sections |
| :---: | :---: | :--- | :---: |
| LTPP | N/A | Asphalt Sections | 87 |
| LTPP | Climatic | Asphalt Sections, Dry/Non-Freeze Climate | 72 |
| LTPP | Region | Asphalt Sections, Dry/Freeze | 15 |
| LTPP | Traffic Level | Asphalt Sections, High Traffic Level (>2000 KESALS) | 44 |
| LTPP |  | 43 |  |

A list of the individual LTPP roadway segments and attributes of each data group is provided in Appendix A: LTPP and MnROAD Analysis.

### 4.3 Data Extraction and Preparation

The pavement data was extracted using the 'Data' tab within LTPP InfoPave. A filtering tool allows for only the data of interest to be selected. After data was selected, it was extracted to a downloadable Microsoft Excel file. In this analysis, one group of data was extracted: Arizona Asphalt Concrete Sections. The extracted Excel file contained the left and right wheel path IRI measurement, the construction number, and the date of measurement. Climate and traffic loading data for each section was collected directly from the LTPP InfoPave website, using the 'Section Summary' tab.

Data extracted from the LTPP database requires manual reformatting to be prepared for analysis. To first simplify the large dataset, the average of the two wheel path readings was used as the sole IRI value for a particular measurement date. The data was then time standardized so all sections began at "Time $=0$ ". Next, all construction numbers were identified, and any series with a new construction number was also standardized to begin at "Time $=0$ ". For all series, the time scale was converted from specific dates to the number of years from the beginning of each series. The individual series were inserted into the modeling spreadsheet for further analysis and model optimization.

### 4.4 Development of Sigmoidal Curves

In this section, the development of sigmoidal curves is explained using the LTPP Asphalt Sections data group as an example. Figure 14 shows each separated series for each asphalt section, which were determined by the construction number, or date in which maintenance was performed. These series were inserted into the modeling spreadsheet to determine the optimal sigmoidal time shift curve. Figure 14 shows this data before any time shifting, with all series beginning at "Time $=0$ ". This data group includes 165 individual series within the 87 pavement sections, which means that on average, there are approximately 2 series per section.


Figure 14: LTPP Data - Raw Asphalt Sections before Time Shifting

The data is optimized to minimize the error between the series and the sigmoidal function.
The fitted sigmoidal curve of the 5 year maximum time shift is provided in Figure 15. The
time shift process is repeated iteratively until the incremental increase of $\mathrm{R}^{2}$ is less than or equal to 0.005 .


Figure 15: LTPP Data - Asphalt Sections, 5 Year Maximum Time Shift

The fitted curves for $10,15,20,25$ and 30 year time shifts are shown in Figures 16, 17, 18, 19 , and 20 , respectively.


Figure 16: LTPP Data - Asphalt Sections, 10 Year Maximum Time Shift


Figure 17: LTPP Data - Asphalt Sections, 15 Year Maximum Time Shift


Figure 18: LTPP Data - Asphalt Sections, 20 Year Maximum Time Shift


Figure 19: LTPP Data - Asphalt Sections, 25 Year Maximum Time Shift


Figure 20: LTPP Data - Asphalt Sections, 30 Year Maximum Time Shift

As the pavement series are allowed a greater maximum time shift, an improved sigmoidal fit is achieved. Modeling efforts did not extend beyond 30 years because a threshold was reached where the measures of model fit no longer increased as the time shift increased. The time shift iteration process is summarized in Figure 21 and Table 8. In Figure 21, the optimized sigmoidal curves of each maximum time shift are superimposed to demonstrate how the shape of the curve changes during the iterative process.


Figure 21: LTPP Data - Time Shift Curves, Asphalt Sections

The model coefficients and measures of fit of each time shift iteration is provided in Table 8. As the maximum allowable time shift increases, the measures of fit ( $\mathrm{Se} / \mathrm{Sy}$ and $\mathrm{R}^{2}$ ) improve until a threshold is reached. This model accuracy was reached at the 25 year time shift. The incremental increase in $R^{2}$ between the 25 and 30 year time shifts was less than 0.005 , which indicates that the threshold was reached. The 25 year time shift was determined to be the optimal time shift, and it is highlighted in Table 8 and Figure 21 in green.

Table 8: LTPP Data - Time Shift Model Coefficients and Measures of Fit, Asphalt Sections

| 5 Year Shift | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  | 30 Year Shift |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.762 | a 1 | 0.828 | a 1 | 0.754 | a 1 | 0.771 | a1 | 0.702 | a 1 | 0.665 |
| a2 | 0.542 | a 2 | 0.915 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 3.045 | a 3 | 1.14 | a 3 | 0.324 | a 3 | 0.301 | a 3 | 0.219 | a 3 | 0.182 |
| a4 | -13.76 | a 4 | -10.094 | a 4 | -5.653 | a 4 | -6.103 | a 4 | -5.082 | a 4 | -4.561 |
| Se/Sy | 0.974 | Se/Sy | 0.812 | Se/Sy | 0.61 | Se/Sy | 0.457 | Se/Sy | 0.397 | Se/Sy | 0.384 |
| R2 | 0.477 | R2 | 0.681 | R2 | 0.835 | R2 | 0.911 | R2 | 0.934 | R2 | 0.938 |

### 4.5 Results

The sigmoidal curve development in Section 4.4 was a demonstration of how the individual series of the asphalt sections were shifted to the optimal location on the deterioration curve.

For each data group listed in Table 8 this process was replicated to determine the optimal time shift curve to best fit the data.

## Climate

Figure 22 and Table 9 depict the comparison of pavement deterioration between roadways in two different climatic regions. In this comparison, the optimal time shift curves have already been determined, and only the final curve is displayed for each data group. The orange dotted line represents the optimal time shift curve for the Dry, Freeze sections, and the blue dotted line represents the optimal time shift curve for the Dry, Non-Freeze sections.


Figure 22: LTPP Asphalt Sections, Climate Comparison

The results of this figure indicate that new pavements in both climatic regions behave very similarly in the first 10 years of pavement life. After this phase, it is observed that the DryFreeze sections deteriorated at a much faster rate (greater slope) than the Dry, Non-Freeze sections. The reduced pavement performance of the Dry, Freeze sections can be attributed to damaging internal freeze-thaw effects repeatedly experienced in pavements within this region.

Table 9: LTPP Asphalt Sections, Climatic Comparison

| Case Study - Comparison: | LTPP - Asphalt Sections - Climatic Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Dry, Non-Freeze | Dry, Freeze |
| Optimal Maximum Time Shift: | 35 | 20 |
| Number of Roadway Sections: | 72 | 15 |
| Number of Data Points: | 707 | 177 |
| Number of Series: | 132 | 34 |
| Se / Sy | 0.390 | 0.238 |
| R2 | 0.936 | 0.977 |
| a1 | 0.608 | 0.729 |
| a2 | 3.500 | 3.500 |
| a3 | 0.142 | 0.338 |
| a4 | -4.090 | -6.472 |

As shown in Table 9, the optimal time shift for the Dry, Non-Freeze and Dry, Freeze sections was determined to be 35 and 20 years, respectively. The lower optimal time shift value of the Dry, Freeze sections also supports the conclusion of a more rapid deterioration pattern. The final sigmoidal curve of each data group showed strong correlation with the respective data series, with $\mathrm{R}^{2}$ values of 0.936 and 0.977 , and $\mathrm{Se} / \mathrm{Sy}$ values of 0.390 and 0.238 .

Figure 23 and Table 10 show the relationship between high and low traffic levels on asphalt pavement sections. Although the lower traffic sections show earlier deterioration, the sections with greater traffic levels show more rapid deterioration.


Figure 23: LTPP Asphalt Sections, Traffic Level Comparison

It is important to note that although these datasets are grouped by traffic level, the other properties within each group may not be consistent. For example, a pavement section may experience greater traffic levels, but also exhibit superior performance over time due to better quality material and structural properties intentionally designed to compensate for the forecasted loading.

A summary of the optimal time shift curves for each traffic loading group is provided in Table 10 Both groups resulted in an optimal time shift of 30 years. A high correlation exists between the fitted sigmoidal curves and the individual data series.

Table 10: LTPP Asphalt Sections, Traffic Loading Comparison

| Case Study - Comparison: | LTPP - Asphalt Sections - Traffic Loading Comparison |  |
| :--- | :---: | :---: |
| Data Set: | AC > 2000 KESALS | AC < 2000 KESALS |
| Optimal Maximum Time Shift: | 30 | 30 |
| Number of Roadway Sections: | 44 | 43 |
| Number of Data Points: | 415 | 469 |
| Number of Series: | 77 | 90 |
| Se / Sy | 0.403 | 0.238 |
| R2 | 0.931 | 0.977 |
| a1 | 0.738 | 0.594 |
| a2 | 3.500 | 3.500 |
| a3 | 0.291 | 0.145 |
| a4 | -7.157 | -3.520 |

The LTPP data shows a practical application of the sigmoidal modeling methodology for IRI data. It was also demonstrated that narrowing the characteristics of the dataset into smaller groups can provide improved model fit. In this case study, the optimal curve of the asphalt sections (Table 8) with an $\mathrm{R}^{2}$ of 0.934 and $\mathrm{Se} / \mathrm{Sy}$ of 0.397 can be considered the baseline model. As the roadway sections were categorized into subgroups, three of the four optimized curves showed improved model correlation. Sorting by climatic region and traffic loading are examples of the subgrouping that could be performed to improve deterioration prediction capabilities.

### 4.6 Summary

The case study utilized data from the LTPP database and focused on asphalt pavement sections located in Arizona. This investigation demonstrated that the sigmoidal function was a suitable model for pavement roughness prediction. Through the analysis of asphalt sections in Arizona, it was shown that the developed sigmoidal curves of some subgroups deteriorated more rapidly than others. Sections located in climates that experience periodic freezing temperatures deteriorated more quickly than sections that did not. It was also
observed that sections with a higher traffic level resulted in higher deterioration; however the other pavement characteristics (e.g., layer material and structure) must be known to ensure the results highlight the desired property rather than a combination of characteristics. In addition, this case study concluded that a more accurate model can be developed by narrowing the selection of pavement sections to a more specific group.

## 5. CASE STUDY 2: MnROAD PAVEMENT ROUGHNESS DATA

### 5.1 Introduction

The Minnesota Road Research Project (MnROAD) is a pavement research facility developed by the Minnesota Department of Transportation. Construction began in 1991, and the completed test track was opened to traffic in 1994 (Tompkins et al 2007). The test track is comprised of individual cells, or pavement sections, with various material, structural, and traffic conditions. The test track was designed as an ongoing experimental study, with 14 primary objectives. Several of the research goals included the evaluation of empirical and mechanistic design methods, the development of mechanistic models, frost prediction modeling, freeze-thaw characteristics, subgrade and subbase performance, and the reliability and variation in pavement performance (Newcomb et al. 1990). There are more than 50 experimental sections, each designed and constructed for a specific research purpose. A 3.5 mile Mainline (interstate) track and a 2.5 mile Low Volume Road track were designed to collect pavement data using over 9,500 sensors located in within the pavement (Tompkins et. al 2007) (Engstrom \& Worel, 2015).The MnROAD test sections are shown in Figure 24 (Tompkins et. al 2007). The MnROAD research facility provides pavement performance data for research use to continue developments in pavement engineering.


Figure 24: MnROAD Test Track Sections (Tompkins et. al 2007)

### 5.2 Data Summary

The IRI data was collected using the Lightweight Inertial Surface Analyzer (LISA). This technology consists of laser profilers and sensors equipped to a utility vehicle. LISA measurements are recorded while the vehicle is in motion. On average, LISA measurements are collected three times per year (MnROAD, 2009). The LISA equipment is regularly calibrated and tested for reliability and accuracy of the data collection.

The pavement roughness data is available on the MnROAD website, using the "MnROAD Data" and "Field Monitoring" links. International roughness index data is available for 95 cells, which includes asphalt, concrete, and composite pavement sections. Some sections were excluded from analysis due to limited sample size. A total of 65 sections were analyzed; 31 asphalt sections, 33 concrete sections, and 3 composite sections. Additional information is provided for the sections, including Roadway Classification, Layer Material (Surface, Base, Subbase), Layer Thickness, Lane Type (Inside/Outside, Driving/Passing), Lane Width, and Drainage information.

For the purpose of this case study, the IRI data of the pavement sections was separated into subgroups based on the pavement type, roadway classification, lane type, lane width, and drainage condition. The goal of the analysis was to demonstrate the sigmoidal curve methodology, and additionally to show that deterioration trends can be observed when comparing multiple related pavement characteristic groups. The modeling process of analyzing and constructing sigmoidal curves was conducted for the following pavement section groups in Table 11.

Table 11: MnROAD Data Grouping Summary

| Data <br> Source | Comparison | Name | Number <br> of <br> Sections |
| :---: | :--- | :--- | :---: |
| MnROAD | Pavement | Asphalt Sections | 31 |
| MnROAD | Type | Composite Sections |  |
| MnROAD |  | Asphalt Low Volume Road Sections | 3 |
| MnROAD |  | Asphalt Mainline Sections | 33 |
| MnROAD | Roadway | 15 |  |
| MnROAD | Classification | Concrete Low Volume Road Sections | 16 |
| MnROAD |  | Concrete Mainline Sections | 14 |
| MnROAD |  | Asphalt Low Volume Road, Inside Lane Sections Low Volume Road, Outside Lane Sections | 19 |
| MnROAD |  | Asphalt Mainline, Driving Lane Sections | 15 |
| MnROAD |  | Concrete Low Volume Road, Inside Lane Sections | 15 |
| MnROAD | Lane Type | Concrete Low Volume Road, Outside Lane Sections | 16 |
| MnROAD |  | Concrete Mainline, Driving Lane Sections | 16 |
| MnROAD |  | Concrete Mainline, Passing Lane Sections | 14 |
| MnROAD |  | Asphalt Low Volume Road, Sections with 12 FT Lane Width | 14 |
| MnROAD |  | Asphalt Low Volume Road, Sections with 13 - 14 FT Lane Width | 8 |
| MnROAD |  | Concrete Mainline, Sections with 12 FT Lane Width | 19 |
| MnROAD |  | Concrete Mainline, Sections with 13-14 FT Lane Width | 14 |
| MnROAD |  | Conerete Mainline, Sections with Drainage | 5 |
| MnROAD |  | Concrete Mainline, Sections without Drainage | 5 |
| MnROAD | Drainage | 14 |  |
| MnROAD | Condition |  | 19 |

A list of the individual MnROAD roadway segments and attributes of each data group is provided in Appendix A.

### 5.3 Data Preparation

The IRI data spreadsheet includes measurements for the left and right wheel path. During each date of measurement, three LISA trials were conducted to ensure reliability of the readings. To prepare the data, the average of the left and right wheel paths was used as the IRI value for each trial. The next step was to determine the average of the three trials on each date of measurement. Each pavement section was simplified to one IRI value for each date.

The process described in the methodology and the LTPP case study was completed for the MnROAD data, where the each section was time standardized to begin at "Time $=0$ ". Significant decreases in IRI value within a roadway section were identified as maintenance intervention, and separated into series, which were also standardized to begin at "Time = 0 ". For all series, the time scale was converted from specific dates to the number of years from the beginning of each series. The individual series were inserted into the modeling spreadsheet for further analysis and model optimization.

### 5.4 Development of Performance Models

In this section, the development of sigmoidal performance curves is explained using the MnROAD Asphalt Sections data group as an example. Figure 25 shows each separated series for each asphalt section, which were determined by the date in which maintenance was performed. These series were inserted into the modeling spreadsheet to determine the optimal sigmoidal time shift curve. Figure 25 shows this data before any time shifting, with all series beginning at "Time $=0$ ". This data group includes 184 individual series within
the 31 pavement sections, which means that on average, there are approximately 6 series per section.


Figure 25: MnROAD Data - Raw Asphalt Sections before Time Shifting

The time shift process is repeated iteratively until the incremental increase of $R^{2}$ is less than or equal to 0.001 . This value is smaller than the threshold increase value used for the LTPP database. This lower threshold value for the MnROAD data is due to higher accuracy of the data. The MnROAD data was collected as part of one research effort, in the same location, using the same equipment, and consistent measurement frequency. The LTPP data was gathered as part of a larger research program and many data collection efforts, using several equipment, and measuring sections slightly less frequently. The results of the MnROAD time shift curves required a more precise incremental increase value, therefore the value of 0.001 was used. The fitted sigmoidal curve of the 5 year maximum time shift is provided in Figure 26.


Figure 26: MnROAD Data - Asphalt Sections, 5 Year Maximum Time Shift

The fitted curves for 10, 15, and 20 year time shifts are shown in Figures 27, 28, and 29, respectively. Similarly to the methodology example and LTPP case study, a better model fit is achieved with a greater maximum time shift, until a threshold accuracy limit is reached.


Figure 27: MnROAD Data - Asphalt Sections, 10 Year Maximum Time Shift


Figure 28: MnROAD Data - Asphalt Sections, 15 Year Maximum Time Shift


Figure 29: MnROAD Data - Asphalt Sections, 20 Year Maximum Time Shift

Modeling efforts did not extend beyond 30 years because a threshold was reached, where the measures of model fit no longer increased as the time shift increased. The time shift iteration process is summarized in Figure 30 and Table 12. In Figure 30, the optimized sigmoidal curves of each maximum time shift are superimposed to demonstrate how the shape of the curve changes during the iterative process.


Figure 30: MnROAD Data - Time Shift Curves, Asphalt Sections

The model coefficients and measures of fit of each time shift iteration is provided in Table 12. As the maximum allowable time shift increases, the measures of fit ( $\mathrm{Se} / \mathrm{Sy}$ and $\mathrm{R}^{2}$ ) improve until a threshold is reached. This model accuracy was reached at the 15 year time shift. The incremental increase in $R^{2}$ between the 15 and 20 year time shifts was less than 0.001 , which indicates that the threshold was reached. The 15 year time shift was determined to be the optimal time shift, and it is highlighted in Table 12 and Figure 30 in green. The fit of the 15 and 20 year time shift is nearly identical, which is why the curves overlap in the figure.

Table 12: MnROAD Data - Time Shift Model Coefficients and Measures of Fit, Asphalt Sections

| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.908 | a1 | 0.846 | a1 | 0.806 | a1 | 0.806 |
| a2 | 3.500 | a2 | 3.500 | a2 | 3.500 | a2 | 3.500 |
| a3 | 0.781 | a3 | 0.528 | a3 | 0.426 | a3 | 0.426 |
| a4 | -4.055 | a4 | -4.189 | a4 | -4.407 | a4 | -4.407 |
| Se/Sy | 0.394 | Se/Sy | 0.288 | Se/Sy | 0.274 | Se/Sy | 0.274 |
| R2 | 0.932 | R2 | 0.964 | R2 | 0.968 | R2 | 0.968 |

### 5.5 Results

The sigmoidal curve development in Section 5.4 was a demonstration of how the individual series of the asphalt sections were shifted to the optimal location on the deterioration curve. For each data group listed in Table 11, this process was replicated to determine the optimal time shift curve to best fit the data. This includes comparisons within the following categories: Pavement Type, Roadway Classification, Lane Type, Lane Width, and Drainage Condition. The curves displayed in these comparison graphs are the determined optimal time shift curve for each data group.

## Pavement Type

Figure 31 and Table 13 depict the comparison of pavement deterioration between roadways of different pavement types. The asphalt and concrete groups resulted in similar performance, however delayed deterioration was observed in the composite sections.


Figure 31: MnROAD Roadway Sections, Pavement Type Comparison

In Table 13, the composite section reached the optimal time shift in 10 years rather than 15 years in the case of asphalt and concrete sections mainly due to the smaller sample size. Due to the limited availability of composite data, this group is excluded from further subgrouping and analysis. The pavement material groups resulted in good correlation between the individual data series and fitted curve, with the best model fit in the Asphalt section group.

Table 13: MnROAD Sections - Pavement Type Comparison

| Case Study - Comparison: | MnROAD - Pavement Type Comparison |  |  |
| :--- | :---: | :---: | :---: |
| Data Set: | Asphalt | Composite | Concrete |
| Optimal Maximum Time Shift: | 15 | 10 | 15 |
| Number of Roadway Sections: | 31 | 3 | 33 |
| Number of Data Points (n): | 1199 | 293 | 1051 |
| Number of Series (p): | 184 | 69 | 180 |
| Se / Sy | 0.274 | 0.317 | 0.362 |
| R2 | 0.968 | 0.961 | 0.944 |
| a1 | 0.806 | 0.467 | 0.802 |
| a2 | 3.500 | 3.500 | 3.500 |
| a3 | 0.426 | 0.518 | 0.393 |
| a4 | -4.407 | -4.416 | -4.243 |

The comparison of pavement type groups demonstrates that by using a large quantity of roadway sections (with various sub-properties), the resulting curves will be general. More detailed modeling is possible when the data group is narrowed to pavement sections with more similar characteristics, which is shown in the next sections of this chapter.

## Roadway Classification

Figure 32 and Table 14 describe the comparison between the various roadway classifications of asphalt pavements. Mainline sections are intended to replicate interstate highways, with more intensive traffic loading but also with stronger pavement materials and structure. The Low Volume Road (LVR) sections are intended to replicate local arterials, with reduced traffic levels and appropriately matched pavement structure. In Figure 32, the Mainline group deteriorated sooner and faster than the LVR group. Although the pavement structure of the Mainline sections are of greater strength and quality, the overwhelming difference in traffic loading is the cause for the Mainline deterioration trends.


Figure 32: MnROAD Asphalt Sections, Roadway Classification Comparison

The sample sizes of each group are similar; however the optimal time shift was determined to be 30 and 15 years for the LVR and Mainline groups, respectively. This indicates that the LVR sections take more time to reach severe deterioration. The model correlation of the two groups, shown in Table 14, which is consistent with the baseline group (Asphalt Sections, Table 12).

Table 14: MnROAD Asphalt Sections, Roadway Classification Comparison

|  | MnROAD - Asphalt Sections - Roadway Classification Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Low Volume Road | Mainline |
| Optimal Maximum Time Shift: | 30 Years | 15 Years |
| Number of Roadway Sections: | 15 | 16 |
| Number of Data Points (n): | 482 | 665 |
| Number of Series (p): | 78 | 103 |
| Se / Sy | 0.289 | 0.241 |
| R2 | 0.964 | 0.975 |
| a1 | 0.702 | 0.776 |
| a2 | 3.500 | 3.500 |
| a3 | 0.232 | 0.454 |
| a4 | -4.543 | -5.296 |

The next comparison of roadway classification is for concrete sections. Figure 33 shows that the Concrete Mainline sections deteriorate more rapidly than the Concrete LVR sections. These findings are consistent with the Asphalt Roadway Classification results, and are also expected to have been caused by the significantly greater traffic loading on Mainline pavements.


Figure 33: MnROAD Concrete Sections, Roadway Classification Comparison

The optimal time shift was determined to be 35 and 15 years for the LVR and Mainline group, respectively. This indicates that the LVR sections require more time to reach severe deterioration. The model correlation of the LVR sections was slightly stronger than the Mainline sections (Table 15).

Table 15: MnROAD Concrete Sections, Roadway Classification Comparison

|  | MnROAD - Concrete Sections - Roadway Classification Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Low Volume Road | Mainline |
| Optimal Maximum Time Shift: | 35 Years | 15 Years |
| Number of Roadway Sections: | 14 | 19 |
| Number of Data Points (n): | 516 | 533 |
| Number of Series (p): | 93 | 89 |
| Se / Sy | 0.275 | 0.418 |
| R2 | 0.968 | 0.924 |
| a1 | 0.976 | 0.781 |
| a2 | 3.500 | 3.500 |
| a3 | 0.308 | 0.470 |
| a4 | -6.991 | -7.715 |

## Lane Type

The next comparison is based on the lane that was measured by the LISA equipment. The right-most lane is generally most utilized due to travel speed considerations and level of access. Highways experience the greatest traffic loading impact in the right-most lane due to slower speeds and high heavy truck utilization. In the United States, it is standard convention to utilize right lanes and reserve left lanes for passing. Similar operation is also observed on local arterials. Right lanes on arterials are also more utilized due to the direct access to complete turns into driveways. In the MnROAD database, different terminology is used for Mainline and LVR sections. IRI data in LVR sections are either Inside (Left) Lanes or Outside (Right) Lanes. The IRI data in Mainline sections is either Passing (Left) Lanes or Driving (Right) Lanes.

The first comparison of Lane Type is for Asphalt LVR sections. Figure 34 shows the deterioration curve for Inside and Outside Lane sections. The Outside (Right) Lane sections are observed to deteriorate earlier in the pavement service life than the Inside (Left) Lane Sections.


Figure 34: MnROAD Asphalt Low Volume Road Sections, Lane Type Comparison

The optimal time shift was determined to be 35 and 20 years for the Inside and Outside Lane groups, respectively. This indicates that the Inside Lane sections required more time to reach severe deterioration. The measures of fit of the Inside and Outside Lane sections, were essentially the same; with $\mathrm{R}^{2}$ values of 0.959 and $\mathrm{Se} / \mathrm{Sy}$ values of 0.310 and 0.308 .

Table 16: MnROAD Asphalt Low Volume Road Sections, Lane Type Comparison

|  | MnROAD - Asphalt Low Volume Road Sections - Lane Type |
| :--- | :---: | :---: |
| Comparison |  |$|$ Outside Lane

The second comparison of Lane Type is for Asphalt Mainline Sections. Figure 35 shows the deterioration curve for Driving and Passing Lane sections. The Driving (Right) Lane sections are observed to deteriorate earlier in the pavement service life than the Passing (Left) Lane Sections.


Figure 35: MnROAD Asphalt Mainline Sections, Lane Type Comparison

The optimal time shift was determined to be 20 and 15 years for the Passing and Driving Lane groups, respectively. This indicates that the Passing Lane sections take more time to reach severe deterioration. The model correlation of the both groups is consistent with the baseline group (Asphalt Mainline Sections, Table 14).

Table 17: MnROAD Asphalt Mainline Sections, Lane Type Comparison

|  | MnROAD - Asphalt Mainline Sections - Lane Type Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Passing Lane | Driving Lane |
| Optimal Maximum Time Shift: | 20 Years | 15 Years |
| Number of Roadway Sections: | 16 | 16 |
| Number of Data Points (n): | 336 | 351 |
| Number of Series (p): | 51 | 54 |
| Se / Sy | 0.247 | 0.259 |
| R2 | 0.974 | 0.971 |
| a1 | 0.710 | 0.958 |
| a2 | 3.500 | 3.500 |
| a3 | 0.362 | 0.644 |
| a4 | -6.100 | -7.955 |

The third comparison of Lane Type is for Concrete LVR sections. Figure 36 shows the deterioration curve for Inside and Outside Lane sections. The Outside Lane and Inside Lanes resulted in very similar deterioration trends. The Outside Lane seems to deteriorate at an earlier date, but the rate of deterioration is greater in the Inside Lane sections.


Figure 36: MnROAD Concrete Low Volume Road Sections, Lane Type Comparison

The optimal time shift was determined to be 15 and 20 years for the Inside and Outside Lane groups, respectively, which is contradictory as to what was observed with the Asphalt LVR Sections. The two Concrete LVR groups deteriorated very similarly, and the results are inconclusive in terms of determining the better performing roadway group. These findings may indicate that the lane distribution has less of an impact for Concrete than Asphalt sections in areas of low traffic.

Table 18: MnROAD Concrete Low Volume Road Sections, Lane Type Comparison

|  | MnROAD - Concrete Low Volume Road Sections - Lane Type Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Inside Lane | Outside Lane |
| Optimal Maximum Time Shift: | 15 Years | 20 Years |
| Number of Roadway Sections: | 14 | 14 |
| Number of Data Points (n): | 259 | 252 |
| Number of Series (p): | 48 | 47 |
| Se / Sy | 0.319 | 0.255 |
| R2 | 0.958 | 0.973 |
| a1 | 1.131 | 0.486 |
| a2 | 3.500 | 3.500 |
| a3 | 0.456 | 0.170 |
| a4 | -6.651 | -2.214 |

The final comparison of Lane Type is for Concrete Mainline sections. Figure 37 shows the deterioration curve for Driving and Passing Lane sections. The results show that both curves begin to deteriorate around the same time, but afterwards the rate of deterioration of the Driving Lane group was greater the deteriorations of the Passing Lane group.


Figure 37: MnROAD Concrete Mainline Sections, Lane Type Comparison

The optimal time shift for both the Passing and Driving Lane groups was determined to be 10 years. This indicates that the Passing Lane sections require more time to reach severe deterioration. The model correlation of the both groups are very similar, and the measures of fit of each group are slightly improved from the baseline group (Concrete Mainline Sections, Table 15).

Table 19: MnROAD Concrete Mainline Sections, Lane Type Comparison

|  | MnROAD - Concrete Mainline Sections - Lane Type Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Passing Lane | Driving Lane |
| Optimal Maximum Time Shift: | 10 Years | 10 Years |
| Number of Roadway Sections: | 19 | 19 |
| Number of Data Points (n): | 264 | 271 |
| Number of Series (p): | 46 | 45 |
| Se / Sy | 0.400 | 0.408 |
| R2 | 0.931 | 0.928 |
| a1 | 0.728 | 0.352 |
| a2 | 3.500 | 3.500 |
| a3 | 0.458 | 0.233 |
| a4 | -5.735 | -2.272 |

In summary, the right (outside or driving) lane was observed to deteriorate more quickly in three of the four comparisons. The results of the Concrete LVR Lane Type comparison were inconclusive, with neither the inside nor outside lane deteriorating at a significantly higher rate. This suggests that the lane distribution does not greatly impact the deterioration of concrete pavements when the traffic level is low.

## Lane Width

The purpose of this comparison is to understand if roughness pavement performance is affected by the lane width of a pavement, and if the pavement type also impacts the findings. The pavement sections were separated into two groups, sections of 12 ft lane widths, and sections with lane widths between 13 and 14 ft . All of the MnROAD sections fit into one of these groups. The idea is that wider lanes may better distribute loading, and that the common wheel path will be less restricted. Also, in concrete pavements wider lanes may minimize the effects of curling and warping. This comparison was conducted for Asphalt LVR sections and Concrete Mainline sections. There was insufficient data to complete the analysis for Asphalt Mainline sections and Concrete LVR sections.

Figure 38 shows the comparison of lane width in Asphalt Low Volume Road sections. The results of this comparison are inconclusive; it cannot be clearly determined that one group deteriorates more rapidly than the other.


Figure 38: MnROAD Asphalt Low Volume Road Sections, Lane Width Comparison

Further information on the model coefficients and fit is provided in Table 20. The results of this comparison suggest that lane width does not have a significant impact on the pavement performance of asphalt sections in low traffic loading conditions.

Table 20: MnROAD Asphalt Low Volume Road Sections, Lane Width Comparison

|  | MnROAD - Asphalt Low Volume Road Sections - Lane Width Comparison |  |
| :--- | :---: | :---: |
| Data Set: | 12 Ft Lane Width | 13 - 14 Lane Width |
| Optimal Maximum Time Shift: | 15 Years | 20 Years |
| Number of Roadway Sections: | 7 | 8 |
| Number of Data Points (n): | 237 | 262 |
| Number of Series (p): | 39 | 41 |
| Se / Sy | 0.400 | 0.253 |
| R2 | 0.930 | 0.973 |
| a1 | 0.701 | 1.297 |
| a2 | 3.500 | 3.500 |
| a3 | 0.343 | 0.592 |
| a4 | -5.750 | -6.603 |

Figure 39 shows the deterioration trend for Concrete Mainline sections of the two lane width groups. In this case, the standard lane width of 12 ft does show greater deterioration than the wider sections of 13-14 ft.


Figure 39: MnROAD Concrete Mainline Sections, Lane Width Comparison

The optimal time shift for both the 12 ft and 13-14 ft lane width groups was determined to be 10 ft . This indicates that the Passing Lane sections take more time to reach severe deterioration. The model correlation of the both groups are consistent are slight improvements from the baseline group (Concrete Mainline Sections, Table 15).

Table 21: MnROAD Concrete Mainline Sections, Lane Width Comparison

|  | MnROAD - Concrete Mainline Sections - Lane Width Comparison |  |
| :--- | :---: | :---: |
| Data Set: | 12 Ft Lane Width | 13-14 Lane Width |
| Optimal Maximum Time Shift: | 10 Years | 10 Years |
| Number of Roadway Sections: | 14 | 5 |
| Number of Data Points (n): | 262 | 266 |
| Number of Series (p): | 47 | 43 |
| Se / Sy | 0.387 | 0.409 |
| R2 | 0.936 | 0.927 |
| a1 | 0.482 | 0.257 |
| a2 | 3.500 | 3.500 |
| a3 | 0.309 | 0.164 |
| a4 | -2.508 | -1.967 |

## By Drainage Condition

The final category used to compare datasets is by the presence of pavement drainage components. The drainage systems in the MnROAD roughness database included wick drains, edge drains, porous pavement systems, open graded base, permeable asphaltstabilized base (with drains), and geocomposite barrier drains. Due to the limited sample size of asphalt sections utilizing these drainage systems, the comparison will focus solely on the comparison of Concrete Mainline sections with and without drainage systems. In Figure 40, the optimal time shift curves for each group is shown. The results demonstrate that concrete sections without drainage systems experience greater deterioration over the pavement life.


Figure 40: MnROAD Concrete Mainline Sections, Drainage Comparison
These findings are also supported by the optimal maximum time shift, which was 20 years for sections with drainage systems, and 10 years for sections without drainage systems.

This indicates that the concrete sections with drainage systems require more time to reach severe deterioration.

Table 22: MnROAD Concrete Mainline Sections, Drainage Comparison

|  | MnROAD - Concrete Mainline Sections - Drainage Comparison |  |
| :--- | :---: | :---: |
| Data Set: | Sections with Drainage | Sections Without Drainage |
| Optimal Maximum Time Shift: | 20 Years | 10 Years |
| Number of Roadway Sections: | 5 | 14 |
| Number of Data Points (n): | 234 | 288 |
| Number of Series (p): | 39 | 52 |
| Se / Sy | 0.306 | 0.380 |
| R2 | 0.960 | 0.939 |
| a1 | 0.202 | 0.734 |
| a2 | 1.817 | 2.561 |
| a3 | 0.230 | 0.583 |
| a4 | -3.000 | -6.333 |

### 5.6 Summary

The second case study included data from the Minnesota Road Research Project, which involves asphalt, concrete, and composite pavement sections. These sections were further grouped into comparison categories of roadway classification, lane type, lane width, and drainage system. By comparing the fitted sigmoidal curves, predicted trends were observed.

In the comparison of pavement material, it was determined that all three pavement types resulted in very similar deterioration curves, but the composite sections' deterioration was slightly delayed and less severe than the asphalt and concrete section groups. The asphalt, concrete, and composite groups resulted in similar curves primarily due to the large volume of pavement sections used in each group, which actually have many diverse characteristics. Based on this first comparison of pavement type, there was interest in further separating the data into finer subgroups, to determine if stronger conclusions and trends could be found.

In the comparison of roadway classification, pavement sections included in the Mainline group (interstate, high traffic loading) deteriorated more quickly than Low Volume Road (LVR) sections. This pattern was observed in both the asphalt and concrete comparisons of roadway classifications. This deterioration trend is due to the higher volumes and greater truck traffic on interstate highways.

Next, the lane type was investigated. This analysis compared primary lanes and secondary lanes on the same roadway sections. Measurements were taken on both the inside/passing lane and the outside/driving lane. After developing the optimal sigmoidal curve for each group, it was determined that the inside/passing lane deteriorates more slowly than the
outside/driving lane. This pattern was observed in Asphalt LVR and Mainline sections, as well as Concrete LVR and Mainline sections.

Pavement groups were also compared by lane width. When comparing the lane widths of Concrete Mainline sections, it was observed that sections with wider lanes (13-14 ft) showed better performance and less deterioration than standard lanes ( 12 ft ). When comparing Asphalt LVR sections, the conclusions were not as distinct. The deterioration curve for each lane width group was similar, indicating that increasing the lane width 1 to 2 inches did not have a significant impact on low volume asphalt roadways.

Lastly, pavement sections were compared to determine the performance differences between Concrete Mainline sections with and without drainage systems. As predicted, the sections without drainage structures showed a higher rate of deterioration which began sooner in the pavement's service life.

Some comparisons showed greater separation between the curves, or deterioration difference between two groups, while other comparisons resulted in very similar curves. Examples of similar curves included the lane type comparison of Concrete LVR sections, and the lane width comparison of Asphalt LVR sections. These results suggest that the comparison property does not significantly impact the IRI pavement performance. Studying deterioration curve separation could be a helpful tool to agencies to identify the characteristics greatly improving pavement performance.

This case study demonstrated the application and suitability of the sigmoidal function in pavement performance modeling.

## 6. SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

### 6.1 Summary

The sigmoidal function is a recognized model form for representing pavement performance. The sigmoidal function has been developed for its implementation in Pavement Condition Index (PCI) modeling and other performance applications. The sigmoidal function captures the three phases of a pavement's life; as the pavement starts in good condition, experiences distresses and deterioration, and reaches a threshold for pavement performance loss.

The objective of this research was to develop a methodology to evaluate and predict pavement roughness over the pavement service life. The goal was to demonstrate the application potential of the sigmoidal function for pavement roughness modeling. The research also aimed to document that separating pavement sections of subgroups of similar characteristics can improve the model accuracy. Lastly, studying the deterioration patterns between comparable subgroups was also of interest. The process used in this methodology to develop sigmoidal curves was validated when comparing two subgroups of different attributes (e.g, pavement type, roadway classification, lane type, lane width, or drainage). This modeling approach provided a prediction tool for pavement roughness conditions if no further maintenance or rehabilitation efforts are employed. Pavement performance is analyzed during the time in between maintenance efforts, to understand how a pavement section within a larger group will behave over time.

### 6.2 Conclusions

Two case studies were included in the research to demonstrate the modeling process and assess the findings. The first case study included data from the Long Term Pavement

Performance (LTPP) InfoPave database. This investigation demonstrated that the sigmoidal function was a suitable model for pavement roughness prediction. Through the analysis of asphalt sections in Arizona, it was demonstrated that the developed sigmoidal curves of some subgroups deteriorated more rapidly than others. Sections located in climates that experience periodic freezing temperatures deteriorated more quickly than sections that did not. In addition, it was concluded that sections with higher traffic levels result in more rapidly deteriorating performance; however, the other pavement characteristics (e.g., layer material and structure) must be known to ensure the data group is only comparing one characteristic, which in this case was traffic loading.

The second case study included data from the Minnesota Road Research Project, which includes asphalt, concrete, and composite pavement sections. These sections were further grouped into comparison categories of roadway classification, lane type, lane width, and drainage system. By comparing the fitted sigmoidal curves, predicted trends were observed. Generally speaking, pavement sections without drainage systems, standard lane widths, a higher roadway classification, or measured in the outermost lane were observed to have more rapid deterioration trends than their counterparts.

The four main conclusions of this research study are as follows:

- The sigmoidal growth performance curve methodology for IRI modeling was successfully demonstrated using data from two major databases (case studies): Long Term Pavement Performance (LTPP) and the Minnesota Department of Transportation MnROAD research program.
- The shifting technique utilized along with the quantity of data from each case study was effective to provide adequate section sample size in each phase of the modeled
performance curve. This is a powerful technique when performance data is not available for all phases of the performance curve.
- Separating IRI data into subgroups of similar pavement characteristics resulted in increased model accuracy.
- The ability to compare IRI performance curves of similar data subgroups was demonstrated, which was useful in providing rationality of trends observed and understanding pavement groups expected to have the most rapid deterioration.


### 6.3 Recommendations

The process of developing the sigmoidal performance function was demonstrated in this study for LTPP and MnROAD data sets. It can be adapted for more specific and practical use by agencies using their sets of collected IRI data. The sigmoidal models have the ability to show the pavement roughness that can be expected over time if there is no maintenance intervention.

It is recommended for agencies to develop more refined models to increase the accuracy of the desired prediction. The modeling efforts in this research serve as a proof of concept of the sigmoidal curve and the methodology. The same framework could be applied to other measures of pavement performance which deteriorate in a similar manner; this could possibly include individual distress, present serviceability rating, and friction loss. In future applications of this framework, it is also possible to model these other performance measures using this methodology and a different mathematical function. Further investigation should be completed to evaluate the suitability of other functions, such as linear or exponential models.

These modeling tools can help an agency allocate funding most effectively by identifying pavement sections or groups that will experience the fastest deterioration. For example, if these pavement sections are identified early, the preventative maintenance budget can be allocated to these sections, while slow deteriorating sections can be identified and maintenance can be delayed. Developing these performance models help to better understand the pavement network and can provide value in asset management and resource allocation planning.

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## APPENDIX A

## LTPP AND MNROAD ANALYSIS

## Roadway Group Dataset Summary

The roadway sections in each dataset group are included in the respective sigmoidal model.
Long Term Pavement Performance (LTPP) InfoPave Database

| Asphalt Sections |  | Asphalt Climatic Comparison |  |  | Asphalt Traffic Comparison |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Dry, Non-Freeze |  | Dry, Freeze | > 2000 KESALS | < 2000 KESALS |
| 0113 | 0903 | 0113 | 1036 | 0603 | 0603 | 0113 |
| 0114 | 1001 | 0114 | 1037 | 0604 | 0604 | 0114 |
| 0115 | 1002 | 0115 | 1062 | 0606 | 0606 | 0115 |
| 0116 | 1003 | 0116 | 1065 | 0607 | 0607 | 0116 |
| 0117 | 1006 | 0117 | 6053 | 0608 | 0608 | 0117 |
| 0118 | 1007 | 0118 | 6054 | 0659 | 0659 | 0118 |
| 0119 | 1015 | 0119 | 6055 | 0660 | 0660 | 0119 |
| 0120 | 1016 | 0120 | 6060 | 0661 | 0661 | 0120 |
| 0121 | 1017 | 0121 | A310 | 0662 | 0662 | 0121 |
| 0122 | 1018 | 0122 | A320 | 0664 | 0664 | 0122 |
| 0123 | 1021 | 0123 | A330 | 0665 | 0665 | 0123 |
| 0124 | 1022 | 0124 | A350 | 0666 | 0666 | 0124 |
| 0161 | 1024 | 0161 | A901 | 0667 | 0667 | 0161 |
| 0162 | 1025 | 0162 | A902 | 0668 | 0668 | 0162 |
| 0163 | 1034 | 0163 | A903 | 0669 | 0669 | 0163 |
| 0260 | 1036 | 0260 | B310 |  | 1003 | 0260 |
| 0261 | 1037 | 0261 | B901 |  | 1006 | 0261 |
| 0501 | 1062 | 0501 | B902 |  | 1007 | 501 |
| 0502 | 1065 | 0502 | B903 |  | 1015 | 502 |
| 0503 | 6053 | 0503 | B959 |  | 1016 | 503 |
| 0504 | 6054 | 0504 | B960 |  | 1017 | 504 |
| 0505 | 6055 | 0505 | B961 |  | 1018 | 505 |
| 0506 | 6060 | 0506 | B964 |  | 1021 | 506 |
| 0507 | A310 | 0507 | C310 |  | 1022 | 507 |
| 0508 | A320 | 0508 | C330 |  | 1024 | 508 |
| 0509 | A330 | 0509 | C340 |  | 1025 | 509 |
| 0559 | A350 | 0559 | C350 |  | 1062 | 559 |
| 0560 | A901 | 0560 | D310 |  | 1065 | 560 |
| 0603 | A902 | 0902 |  |  | 6053 | 902 |
| 0604 | A903 | 0903 |  |  | 6054 | 903 |
| 0606 | B310 | 1001 |  |  | 6055 | 1002 |
| 0607 | B901 | 1002 |  |  | B310 | 1034 |
| 0608 | B902 | 1003 |  |  | B901 | 1036 |
| 0659 | B903 | 1006 |  |  | B902 | 1037 |
| 0660 | B959 | 1007 |  |  | B903 | 6060 |
| 0661 | B960 | 1015 |  |  | B959 | A310 |
| 0662 | B961 | 1016 |  |  | B960 | A320 |
| 0664 | B964 | 1017 |  |  | B961 | A330 |
| 0665 | C310 | 1018 |  |  | B964 | A330 |
| 0666 | C330 | 1021 |  |  | C310 | A350 |
| 0667 | C340 | 1022 |  |  | C330 | A901 |
| 0668 | C350 | 1024 |  |  | C340 | A902 |
| 0669 | D310 | 1025 |  |  | C350 | A903 |
| 0902 |  | 1034 |  |  | D310 |  |


| Data Set Title: | Asphalt Sections |
| :--- | :--- |
| Case Study: | 1 |
| Data Source: | LTPP |
| Number of Sections: | 87 |
| Number of Data Points (n): | 884 |
| Number of Series (p): | 165 |
| Optimal Maximum Time Shift: | 25 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.76236 | a1 | 0.82824 | a 1 | 0.75436 | a1 | 0.77144 | a1 | 0.70178 |
| a2 | 0.54158 | a2 | 0.9152 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 3.04457 | a3 | 1.14042 | a3 | 0.32437 | a3 | 0.30077 | a3 | 0.21877 |
| a4 | -13.76 | a4 | -10.094 | a4 | -5.6529 | a4 | -6.103 | a4 | -5.0823 |
| Se/Sy | 0.97416 | Se/Sy | 0.81187 | Se/Sy | 0.60964 | Se/Sy | 0.45654 | Se/Sy | 0.39733 |
| R2 | 0.47673 | R2 | 0.68065 | R2 | 0.83509 | R2 | 0.9112 | R2 | 0.93352 |


| 30 Year Shift |  |
| :---: | :---: |
| a1 | 0.66535 |
| a2 | 3.5 |
| a3 | 0.18238 |
| a4 | -4.5607 |
| Se/Sy | 0.38371 |
| R2 | 0.93814 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Dry Non-Freeze Climatic Sections |
| :--- | :--- |
| Case Study: | 1 |
| Data Source: | LTPP |
| Number of Sections: | 72 |
| Number of Data Points (n): | 707 |
| Number of Series (p): | 132 |
| Optimal Maximum Time Shift: | 35 |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3}{ }^{* t+a_{4}}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  |  | 20 Year Shift |  | 25 Year Shift |  |  |
| :---: | :---: | :---: | :---: | :--- | :--- | :--- | :---: | :---: | :---: |
| a1 | 0.77283 | a1 | 0.82937 |  |  | a1 | 0.7693 | a1 | 0.70631 |
| a2 | 0.5149 | a2 | 0.88583 |  |  | a2 | 3.5 | a2 | 3.5 |
| a3 | 10.5226 | a3 | 1.1639 |  |  | a3 | 0.31477 | a3 | 0.22357 |
| a4 | -50.816 | a4 | -10.617 |  |  | a4 | -6.4515 | a4 | -5.3147 |
| Se/Sy | 0.97255 | Se/Sy | 0.83079 |  |  | Se/Sy | 0.49434 | Se/Sy | 0.42868 |
| R2 | 0.47921 | R2 | 0.66171 |  |  | R2 | 0.89497 | R2 | 0.92213 |


| 30 Year Shift |  | 35 Year Shift |  |  |  |
| :---: | :---: | :---: | :---: | :--- | :--- |
| a1 | 0.64046 | a1 | 0.60823 |  |  |
| a2 | 3.5 | a2 | 3.5 |  |  |
| a3 | 0.16976 | a3 | 0.14169 |  |  |
| a4 | -4.357 | a4 | -4.09 |  |  |
| Se/Sy | 0.40649 | Se/Sy | 0.38976 |  |  |
| R2 | 0.93028 | R2 | 0.93609 |  |  |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Dry Freeze Climatic Sections |
| :--- | :--- |
| Case Study: | 1 |
| Data Source: | LTPP |
| Number of Sections: | 15 |
| Number of Data Points (n): | 177 |
| Number of Series (p): | 34 |
| Optimal Maximum Time Shift: | 20 |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3}{ }^{* t+a_{4}}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.84773 | a1 | 0.86724 | a1 | 0.74266 | a1 | 0.72921 | a1 | 0.73558 |
| a2 | 0.60641 | a2 | 1.40406 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 11.02 | a3 | 2.60063 | a3 | 0.43811 | a3 | 0.33849 | a3 | 0.30882 |
| a4 | -48.143 | a4 | -24.911 | a4 | -6.523 | a4 | -6.4724 | a4 | -7.3697 |
| Se/Sy | 0.92313 | Se/Sy | 0.49623 | Se/Sy | 0.29053 | Se/Sy | 0.23792 | Se/Sy | 0.22829 |
| R2 | 0.55463 | R2 | 0.89438 | R2 | 0.9651 | R2 | 0.97673 | R2 | 0.9786 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Sections, Greater than 2000 KESALS |
| :--- | :--- |
| Case Study: | 1 |
| Data Source: | LTPP |
| Number of Sections: | 44 |
| Number of Data Points (n): | 415 |
| Number of Series (p): | 77 |
| Optimal Maximum Time Shift: | 30 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.68727 | a1 | 0.78672 | a1 | 0.74926 | a1 | 0.76689 | a1 | 0.74515 |
| a2 | 0.50344 | a2 | 0.80766 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 1.74763 | a3 | 1.65097 | a3 | 0.39829 | a3 | 0.35056 | a3 | 0.27799 |
| a4 | -7.4384 | a4 | -15.409 | a4 | -7.0901 | a4 | -6.9955 | a4 | -6.4515 |
| Se/Sy | 1.00276 | Se/Sy | 0.83658 | Se/Sy | 0.65786 | Se/Sy | 0.47649 | Se/Sy | 0.42386 |
| R2 | 0.42316 | R2 | 0.65468 | R2 | 0.80416 | R2 | 0.90257 | R2 | 0.92375 |


| 30 Year Shift |  | 35 Year Shift |  |
| :---: | :---: | :---: | :---: |
| a1 | 0.73803 | a1 | 0.72889 |
| a2 | 3.5 | a2 | 3.5 |
| a3 | 0.29075 | a3 | 0.28659 |
| a4 | -7.1571 | a4 | -7.3651 |
| Se/Sy | 0.4028 | Se/Sy | 0.39415 |
| R2 | 0.93142 | R2 | 0.93443 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Sections, Less than 2000 KESALS |
| :--- | :--- |
| Case Study: | 1 |
| Data Source: | LTPP |
| Number of Sections: | 43 |
| Number of Data Points (n): | 469 |
| Number of Series (p): | 90 |
| Optimal Maximum Time Shift: | 30 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.72472 | a1 | 0.86101 | a 1 | 0.80427 | a 1 | 0.72501 | a1 | 0.68545 |
| a2 | 0.85227 | a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a2 | 3.5 |
| a3 | 0.65266 | a3 | 0.47266 | a 3 | 0.32629 | a 3 | 0.22446 | a3 | 0.18942 |
| a4 | -3.1631 | a4 | -5.7675 | a4 | -5.0146 | a4 | -4.177 | a4 | -4.237 |
| Se/Sy | 0.95576 | Se/Sy | 0.64976 | Se/Sy | 0.48085 | Se/Sy | 0.40989 | Se/Sy | 0.365 |
| R2 | 0.51013 | R2 | 0.81124 | R2 | 0.90153 | R2 | 0.92949 | R2 | 0.94452 |


| 30 Year Shift |  | 35 Year Shift |  |
| :---: | :---: | :---: | :---: |
| a1 | 0.59444 | a1 | 0.54045 |
| a2 | 3.5 | a2 | 3.5 |
| a3 | 0.14542 | a3 | 0.12975 |
| a4 | -3.5204 | a4 | -3.2296 |
| Se/Sy | 0.34642 | Se/Sy | 0.34148 |
| R2 | 0.95017 | R2 | 0.95161 |

Note: Green shading represents the optimal maximum time shift

## Roadway Group Dataset Summary

The roadway sections in each dataset group are included in the respective sigmoidal model.
Minnesota Department of Transportation MnROAD Database

| Pavement Type* |  |  | Asphalt Roadway Classification* |  | Concrete Road Classification* |  | Concrete Mainline Sections* |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asphalt | Composite | Concrete | Low Volume Road | Mainline | Low Volume Road | Mainline | With Drainage | Without Drainage |
| 1 | 92 | 5 | 24 | 1 | 32 | 5 | 7 | 5 |
| 2 | 93 | 6 | 25 | 2 | 36 | 6 | 8 | 6 |
| 3 | 94 | 7 | 26 | 3 | 37 | 7 | 9 | 11 |
| 4 | 95 | 8 | 27 | 4 | 38 | 8 | 10 | 13 |
| 14 | 96 | 9 | 28 | 14 | 39 | 9 | 12 | 60 |
| 15 | 97 | 10 | 29 | 15 | 40 | 10 |  | 61 |
| 16 |  | 11 | 30 | 16 | 41 | 11 |  | 62 |
| 17 |  | 12 | 31 | 17 | 42 | 12 |  | 63 |
| 18 |  | 13 | 33 | 18 | 43 | 13 |  | 114 |
| 19 |  | 32 | 34 | 19 | 44 | 60 |  | 213 |
| 20 |  | 36 | 35 | 20 | 45 | 61 |  | 214 |
| 21 |  | 37 | 54 | 21 | 46 | 62 |  | 414 |
| 22 |  | 38 | 77 | 22 | 52 | 63 |  | 513 |
| 23 |  | 39 | 78 | 23 | 53 | 114 |  | 614 |
| 24 |  | 40 | 79 | 50 |  | 213 |  |  |
| 25 |  | 41 |  | 51 |  | 214 |  |  |
| 26 |  | 42 |  |  |  | 414 |  |  |
| 27 |  | 43 |  |  |  | 513 |  |  |
| 28 |  | 44 |  |  |  | 614 |  |  |
| 29 |  | 45 |  |  |  |  |  |  |
| 30 |  | 46 |  |  |  |  |  |  |
| 31 |  | 52 |  |  |  |  |  |  |
| 33 |  | 53 |  |  |  |  |  |  |
| 34 |  | 60 |  |  |  |  |  |  |
| 35 |  | 61 |  |  |  |  |  |  |
| 50 |  | 62 |  |  |  |  |  |  |
| 51 |  | 63 |  |  |  |  |  |  |
| 54 |  | 114 |  |  |  |  |  |  |
| 77 |  | 213 |  |  |  |  |  |  |
| 78 |  | 214 |  |  |  |  |  |  |
| 79 |  | 414 |  |  |  |  |  |  |
|  |  | 513 |  |  |  |  |  |  |
|  |  | 614 |  |  |  |  |  |  |

*Note: These grouped sections include both lane types. The Low Volume Road sections include the inside and outside lanes, and the Mainline sections include the driving and passing lanes.

## Roadway Group Dataset Summary

The roadway sections in each dataset group are included in the respective sigmoidal model.

## Minnesota Department of Transportation MnROAD Database

| Asphalt Low Volume Road |  | Asphalt Mainline |  | Concrete Low <br> Volume Road |  | Concrete Mainline |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Outside } \\ & \text { Lane } \\ & \text { Sections } \end{aligned}$ |  | Passing <br> Lane <br> Sections |  | Outside Lane Sections | Driving <br> Lane <br> Sections | Passing <br> Lane <br> Sections |
| 24 - I | 24-O | $1-\mathrm{D}$ | 1 - P | 32 - I | 32-O | $5-\mathrm{D}$ | 5 - P |
| 25 - I | $25-\mathrm{O}$ | 2 - D | 2 - P | 36 - I | $36-\mathrm{O}$ | 6 - D | 6 - P |
| 26 - I | 26-O | $3-\mathrm{D}$ | $3-\mathrm{P}$ | 37 - I | 37-O | 7 - D | $7-\mathrm{P}$ |
| 27 - I | 27-O | 4 - D | $4-\mathrm{P}$ | 38 - I | 38-O | 8 - D | $8-\mathrm{P}$ |
| 28 - I | $28-\mathrm{O}$ | 14 - D | 14 - P | 39 - I | 39-O | $9-\mathrm{D}$ | $9-\mathrm{P}$ |
| 29 - I | 29-O | 15 - D | $15-\mathrm{P}$ | 40 - I | 40-O | $10-\mathrm{D}$ | $10-\mathrm{P}$ |
| $30-\mathrm{I}$ | 30-0 | 16 - D | 16 - P | 41 - I | 41-O | $11-\mathrm{D}$ | $11-\mathrm{P}$ |
| $31-\mathrm{I}$ | $31-\mathrm{O}$ | 17 - D | 17 - P | 42 - I | 42-O | 12 - D | 12 - P |
| 33 - I | 33-0 | 18 - D | 18 - P | 43 - I | 43-0 | 13 - D | 13 - P |
| 34 - I | 34-O | 19 - D | 19 - P | 44 - I | 44-O | 60 - D | $60-\mathrm{P}$ |
| $35-\mathrm{I}$ | 35-O | 20 - D | $20-\mathrm{P}$ | 45 - I | 45-O | $61-\mathrm{D}$ | $61-\mathrm{P}$ |
| 54 - I | 54-O | 21 - D | $21-\mathrm{P}$ | 46 - I | $46-\mathrm{O}$ | 62 - D | 62 - P |
| 77 - I | 77-0 | 22 - D | $22-\mathrm{P}$ | 52 - I | 52-O | 63 - D | 63 - P |
| 78 - I | 78-O | 23 - D | 23 - P | 53 - I | 53-0 | 114 - D | $114-\mathrm{P}$ |
| 79 - I | 79-0 | $50-\mathrm{D}$ | $50-\mathrm{P}$ |  |  | 213-D | $213-\mathrm{P}$ |
|  |  | 51 - D | $51-\mathrm{P}$ |  |  | 214 - D | 214 - P |
|  |  |  |  |  |  | 414 - D | 414 - P |
|  |  |  |  |  |  | 513 - D | $513-\mathrm{P}$ |
|  |  |  |  |  |  | 614 - D | $614-\mathrm{P}$ |
|  |  |  |  |  |  |  |  |
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Note: A particular roadway segment can be further defined by the inside (passing) or outside (driving) lane. MnROAD uses different terminology based on the roadway classification. Low Volume Road sections are defined by either "Inside Lane" or "Outside Lane", and Mainline sections are defined by either "Driving Lane" or "Passing Lane".

## Roadway Group Dataset Summary

The roadway sections in each dataset group are included in the respective sigmoidal model.

## Minnesota Department of Transportation MnROAD Database

| Asphalt Low <br> Volume Road* |  | Concrete Mainline* |  |
| :---: | :---: | :---: | :---: |
| 12 Ft <br> Lane <br> Width | $13-14 \mathrm{Ft}$ <br> Lane <br> Width | 12 Ft <br> Lane <br> Width | $13-14 \mathrm{Ft}$ <br> Lane <br> Width |
| 24 | 27 | 10 | 5 |
| 25 | 28 | 11 | 6 |
| 26 | 33 | 12 | 7 |
| 29 | 34 | 13 | 8 |
| 30 | 35 | 60 | 9 |
| 31 | 77 | 61 |  |
| 54 | 78 | 62 |  |
|  | 79 | 63 |  |
|  |  | 114 |  |
|  |  | 213 |  |
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*Note: These grouped sections include both lane types. The Low Volume Road sections include the inside and outside lanes, and the Mainline sections include the driving and passing lanes.

| Data Set Title: | Asphalt Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 31 |
| Number of Data Points (n): | 1199 |
| Number of Series (p): | 184 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.90816 | a 1 | 0.84593 | a 1 | 0.80623 | a 1 | 0.80828 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 0.7814 | a 3 | 0.52769 | a 3 | 0.42619 | a 3 | 0.42008 |
| N4te: Green shading |  |  |  |  |  |  |  |
| represents the optimal |  |  |  |  |  |  |  |
| maximum time shift |  |  |  |  |  |  |  |



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.4801 | a1 | 0.46705 | a1 | 0.46688 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.61036 | a3 | 0.51808 | a3 | 0.51785 |
| a4 | -2.6117 | a4 | -4.4161 | a4 | -5.2829 |
| Se/Sy | 0.32267 | Se/Sy | 0.31681 | Se/Sy | 0.31681 |
| R2 | 0.95924 | R2 | 0.96073 | R2 | 0.96073 |

Note: Green shading represents the optimal maximum time shift


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.86087 | a1 | 0.78869 | a1 | 0.80188 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.6504 | a3 | 0.42077 | a3 | 0.39305 |
| a4 | -3.6962 | a4 | -3.7471 | a4 | -4.2428 |
| Se/Sy | 0.43342 | Se/Sy | 0.36533 | Se/Sy | 0.36223 |
| R2 | 0.91879 | R2 | 0.94302 | R2 | 0.94401 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Low Volume Road Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 15 |
| Number of Data Points (n): | 482 |
| Number of Series (p): | 78 |
| Optimal Maximum Time Shift: | 30 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.02359 | a1 | 0.84524 | a 1 | 0.75627 | a 1 | 0.72101 | a 1 | 0.70471 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 0.89777 | a 3 | 0.46662 | a 3 | 0.34 | a 3 | 0.28211 | a3 | 0.24933 |
| a4 | -4.9165 | a4 | -3.8038 | a4 | -3.6136 | a4 | -3.7461 | a4 | -4.0249 |
| Se/Sy | 0.52078 | Se/Sy | 0.35112 | Se/Sy | 0.31027 | Se/Sy | 0.29582 | Se/Sy | 0.29033 |
| R2 | 0.87875 | R2 | 0.94681 | R2 | 0.95872 | R2 | 0.96255 | R2 | 0.96395 |


| 30 Year Shift |  | 35 Year Shift |  |
| :---: | :---: | :---: | :---: |
| a1 | 0.70171 | a1 | 0.70171 |
| a2 | 3.5 | a2 | 3.5 |
| a3 | 0.2319 | a3 | 0.2319 |
| a4 | -4.5431 | a4 | -4.5431 |
| Se/Sy | 0.2885 | Se/Sy | 0.2885 |
| R2 | 0.96441 | R2 | 0.96441 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Mainline Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 16 |
| Number of Data Points (n): | 665 |
| Number of Series (p): | 103 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3^{*}} t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Note: Green shading |  |  |  |  |  |  |  |
|  | 0.7163 | a 1 | 0.73912 | a 1 | 0.77642 | a 1 | 0.75868 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.2954 |
| a3 | 0.62746 | a 3 | 0.4751 | a 3 | 0.45419 | a 3 | 0.40601 |
| represents the optimal |  |  |  |  |  |  |  |
| maximum time shift |  |  |  |  |  |  |  |


| Data Set Title: | Concrete Low Volume Road Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 14 |
| Number of Data Points (n): | 516 |
| Number of Series (p): | 93 |
| Optimal Maximum Time Shift: | 35 Years |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3}{ }^{*} t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.15559 | a 1 | 1.05269 | a 1 | 1.0104 | a 1 | 0.99637 | a 1 | 0.9897 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 0.82166 | a 3 | 0.52672 | a 3 | 0.41332 | a 3 | 0.3593 | a 3 | 0.33127 |
| a4 | -4.045 | a 4 | -3.9275 | a 4 | -4.2156 | a 4 | -4.6784 | a 4 | -5.3143 |
| Se/Sy | 0.41512 | Se/Sy | 0.31864 | Se/Sy | 0.29042 | Se/Sy | 0.28054 | Se/Sy | 0.27701 |
| R2 | 0.92653 | R2 | 0.9574 | R2 | 0.96474 | R2 | 0.96714 | R2 | 0.96797 |


| 30 Year Shift |  | 35 Year Shift |  | 40 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.98145 | a1 | 0.97619 | a1 | 0.97619 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.31612 | a3 | 0.30834 | a3 | 0.30834 |
| a4 | -6.0764 | a4 | -6.9908 | a4 | -6.9908 |
| Se/Sy | 0.27574 | Se/Sy | 0.27529 | Se/Sy | 0.27529 |
| R2 | 0.96827 | R2 | 0.96838 | R2 | 0.96838 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Mainline Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 19 |
| Number of Data Points (n): | 533 |
| Number of Series (p): | 89 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process:
$I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | Note: Green shading represents the optimal maximum time shift |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.78073 | a1 | 0.7719 | a1 | 0.78133 | a1 | 0.77971 |  |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |  |
| a3 | 0.57909 | a3 | 0.46797 | a3 | 0.46998 | a3 | 0.46854 |  |
| a4 | -3.9116 | a4 | -5.3366 | a4 | -7.7151 | a4 | -9.8956 |  |
| Se/Sy | 0.44084 | Se/Sy | 0.4189 | Se/Sy | 0.41839 | Se/Sy | 0.41835 |  |
| R2 | 0.91532 | R2 | 0.92388 | R2 | 0.92407 | R2 | 0.92409 |  |


| Data Set Title: | Concrete Mainline Sections, with Drainage |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 5 |
| Number of Data Points (n): | 234 |
| Number of Series (p): | 39 |
| Optimal Maximum Time Shift: | 20 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3}{ }^{* t+a_{4}}\right.}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.66607 | a1 | 0.58211 | a1 | 0.44765 | a1 | 0.20182 | a1 | 0.20182 |
| a2 | 3.5 | a2 | 3.49404 | a2 | 3.49906 | a2 | 1.81706 | a2 | 1.81706 |
| a3 | 0.37181 | a3 | 0.21639 | a3 | 0.15922 | a3 | 0.2299 | a3 | 0.2299 |
| a4 | -3 | a4 | -3 | a4 | -3 | a4 | -3 | a4 | -3 |
| Se/Sy | 0.42027 | Se/Sy | 0.32576 | Se/Sy | 0.3132 | Se/Sy | 0.30617 | Se/Sy | 0.30617 |
| R2 | 0.92314 | R2 | 0.95456 | R2 | 0.95807 | R2 | 0.95997 | R2 | 0.95997 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Mainline Sections, without Drainage |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 14 |
| Number of Data Points (n): | 288 |
| Number of Series (p): | 52 |
| Optimal Maximum Time Shift: | 10 Years |

Plot of Time Shifting Process:
$I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.72759 | a1 | 0.73381 | a1 | 0.73584 |
| a2 | 2.49833 | a2 | 2.56137 | a2 | 2.54866 |
| a3 | 0.61572 | a3 | 0.58296 | a3 | 0.58573 |
| a4 | -3.6679 | a4 | -6.3327 | a4 | -8.9895 |
| Se/Sy | 0.38398 | Se/Sy | 0.37991 | Se/Sy | 0.37991 |
| R2 | 0.93742 | R2 | 0.93878 | R2 | 0.93879 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Low Volume Road - Inside Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 15 |
| Number of Data Points (n): | 216 |
| Number of Series (p): | 36 |
| Optimal Maximum Time Shift: | 35 Years |

Plot of Time Shifting Process:
$I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.09242 | a 1 | 0.99359 | a 1 | 0.93435 | a 1 | 0.90604 | a 1 | 0.8927 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a 3 | 1.39559 | a 3 | 0.76046 | a 3 | 0.54822 | a 3 | 0.44938 | a 3 | 0.3918 |
| a4 | -6.68 | a 4 | -4.9925 | a 4 | -4.9044 | a 4 | -5.0947 | a 4 | -5.3782 |
| Se/Sy | 0.53201 | Se/Sy | 0.37196 | Se/Sy | 0.34088 | Se/Sy | 0.32563 | Se/Sy | 0.31747 |
| R2 | 0.87352 | R 2 | 0.9403 | R 2 | 0.95011 | R2 | 0.95458 | R 2 | 0.95688 |


| 30 Year Shift |  | 35 Year Shift |  | 40 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.88398 | a1 | 0.87883 | a1 | 0.87556 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.35398 | a3 | 0.32757 | a3 | 0.30862 |
| a4 | -5.7114 | a4 | -6.0791 | a4 | -6.4804 |
| Se/Sy | 0.31288 | Se/Sy | 0.3102 | Se/Sy | 0.30861 |
| R2 | 0.95815 | R2 | 0.95887 | R2 | 0.9593 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Low Volume Road - Outside Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 15 |
| Number of Data Points (n): | 277 |
| Number of Series (p): | 45 |
| Optimal Maximum Time Shift: | 20 Years |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.15223 | a 1 | 1.0248 | a 1 | 0.95937 | a 1 | 0.94971 | a 1 | 0.94971 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 1.08724 | a 3 | 0.56441 | a 3 | 0.3978 | a 3 | 0.34454 | a 3 | 0.34454 |
| a4 | -6.0493 | a 4 | -4.7432 | a 4 | -4.5735 | a 4 | -5.0975 | a 4 | -5.0975 |
| Se/Sy | 0.51947 | Se/Sy | 0.33764 | Se/Sy | 0.31129 | Se/Sy | 0.30835 | Se/Sy | 0.30835 |
| R2 | 0.8793 | R2 | 0.95088 | R2 | 0.95841 | R2 | 0.95921 | R2 | 0.95921 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Mainline - Driving Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 16 |
| Number of Data Points (n): | 351 |
| Number of Series (p): | 54 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Note: Green shading |  |  |  |  |  |  |  |
|  | 0.97933 | a 1 | 0.95087 | a 1 | 0.95834 | a 1 | 0.95244 |
| a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 0.97422 | a 3 | 0.68542 | a 3 | 0.64365 | a 3 | 0.64175 |
| represents the optimal |  |  |  |  |  |  |  |
| maximum time shift |  |  |  |  |  |  |  |


| Data Set Title: | Asphalt Mainline - Passing Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 16 |
| Number of Data Points (n): | 336 |
| Number of Series (p): | 51 |
| Optimal Maximum Time Shift: | 20 Years |

Plot of Time Shifting Process:
$I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.68661 | a1 | 0.6589 | a 1 | 0.67573 | a 1 | 0.70968 | a 1 | 0.70968 |
| a2 | 3.5 | a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 0.59855 | a3 | 0.4212 | a 3 | 0.36113 | a 3 | 0.36215 | a 3 | 0.36215 |
| a4 | -2.9766 | a4 | -3.2842 | a4 | -4.2273 | a4 | -6.0996 | a4 | -6.0996 |
| Se/Sy | 0.34926 | Se/Sy | 0.25838 | Se/Sy | 0.24714 | Se/Sy | 0.24665 | Se/Sy | 0.24665 |
| R2 | 0.94669 | R2 | 0.97119 | R2 | 0.97367 | R2 | 0.97378 | R2 | 0.97378 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Low Volume Road - Inside Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 14 |
| Number of Data Points (n): | 259 |
| Number of Series (p): | 48 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.16957 | a1 | 1.12931 | a1 | 1.13062 | a1 | 1.13117 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.71219 | a3 | 0.49434 | a3 | 0.45645 | a3 | 0.45032 |
| a4 | -3.7956 | a4 | -4.7909 | a4 | -6.6509 | a4 | -8.8061 |
| Se/Sy | 0.36274 | Se/Sy | 0.32298 | Se/Sy | 0.31883 | Se/Sy | 0.31837 |
| R2 | 0.94466 | R2 | 0.95639 | R2 | 0.95753 | R2 | 0.95765 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Low Volume Road - Outside Lane Section |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 14 |
| Number of Data Points (n): | 252 |
| Number of Series (p): | 47 |
| Optimal Maximum Time Shift: | 20 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.67255 | a1 | 0.34725 | a1 | 0.43472 | a1 | 0.48638 | a1 | 0.48638 |
| a2 | 2.34099 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.56371 | a3 | 0.24045 | a3 | 0.17863 | a3 | 0.16951 | a3 | 0.16951 |
| a4 | -2.1263 | a4 | -1.8367 | a4 | -2.0597 | a4 | -2.214 | a4 | -2.214 |
| Se/Sy | 0.38443 | Se/Sy | 0.27313 | Se/Sy | 0.25571 | Se/Sy | 0.25531 | Se/Sy | 0.25531 |
| R2 | 0.93771 | R2 | 0.96906 | R2 | 0.97293 | R2 | 0.97302 | R2 | 0.97302 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Mainline - Driving Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 19 |
| Number of Data Points (n): | 271 |
| Number of Series (p): | 45 |
| Optimal Maximum Time Shift: | 10 Years |

Plot of Time Shifting Process:


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.14878 | a1 | 0.35215 | a1 | 0.35215 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.25896 | a3 | 0.23293 | a3 | 0.23293 |
| a4 | -1.5913 | a4 | -2.2716 | a4 | -2.2716 |
| Se/Sy | 0.43108 | Se/Sy | 0.40821 | Se/Sy | 0.40821 |
| R2 | 0.91938 | R2 | 0.92803 | R2 | 0.92803 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Concrete Mainline - Passing Lane Sections |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 19 |
| Number of Data Points (n): | 264 |
| Number of Series (p): | 46 |
| Optimal Maximum Time Shift: | 10 Years |

Plot of Time Shifting Process:


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.69717 | a1 | 0.7284 | a1 | 0.7284 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.47757 | a3 | 0.45848 | a3 | 0.45848 |
| a4 | -3.5699 | a4 | -5.7347 | a4 | -5.7347 |
| Se/Sy | 0.40581 | Se/Sy | 0.40024 | Se/Sy | 0.40024 |
| R2 | 0.92925 | R2 | 0.93124 | R2 | 0.93124 |

Note: Green shading represents the optimal maximum time shift

| Data Set Title: | Asphalt Low Volume Road - 12 Ft Lane Width |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 7 |
| Number of Data Points (n): | 237 |
| Number of Series (p): | 39 |
| Optimal Maximum Time Shift: | 15 Years |

Plot of Time Shifting Process: $I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}$


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | Note: Green shading represents the optimal maximum time shift |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.55757 | a1 | 0.64381 | a1 | 0.70146 | a1 | 0.70802 |  |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |  |
| a3 | 0.44012 | a3 | 0.33542 | a3 | 0.34258 | a3 | 0.34396 |  |
| a4 | -2.926 | a4 | -3.9085 | a4 | -5.7504 | a4 | -7.496 |  |
| Se/Sy | 0.45633 | Se/Sy | 0.40185 | Se/Sy | 0.40042 | Se/Sy | 0.4003 |  |
| R2 | 0.90845 | R2 | 0.9298 | R2 | 0.93031 | R2 | 0.93036 |  |


| Data Set Title: | Asphalt Low Volume Road - 13 or 14 Ft Lane Widt |
| :--- | :--- |
| Case Study: | 2 |
| Data Source: | MnRoad |
| Number of Sections: | 8 |
| Number of Data Points (n): | 262 |
| Number of Series (p): | 41 |
| Optimal Maximum Time Shift: | 20 Years |

Plot of Time Shifting Process:

$$
I R I=a_{1}+\frac{a_{2}}{1+e^{\left(-a_{3} * t+a_{4}\right)}}
$$



| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  | 20 Year Shift |  | 25 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 1.45664 | a1 | 1.34384 | a 1 | 1.31029 | a 1 | 1.29654 | a 1 | 1.2904 |
| a2 | 3.5 | a2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 | a 2 | 3.5 |
| a3 | 2.59131 | a3 | 0.97867 | a 3 | 0.7098 | a 3 | 0.59179 | a3 | 0.52907 |
| a4 | -12.814 | a4 | -6.6332 | a4 | -6.3295 | a4 | -6.6029 | a4 | -7.1333 |
| Se/Sy | 0.48734 | Se/Sy | 0.28371 | Se/Sy | 0.26026 | Se/Sy | 0.25257 | Se/Sy | 0.2496 |
| R2 | 0.89381 | R2 | 0.96532 | R2 | 0.9709 | R2 | 0.97262 | R2 | 0.97327 |

Note: Green shading represents the optimal maximum time shift


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.49056 | a1 | 0.48182 | a1 | 0.4818 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.34443 | a3 | 0.30887 | a3 | 0.30886 |
| a4 | -2.4597 | a4 | -2.5081 | a4 | -2.5081 |
| Se/Sy | 0.39938 | Se/Sy | 0.38681 | Se/Sy | 0.38681 |
| R2 | 0.93199 | R2 | 0.93635 | R2 | 0.93635 |

Note: Green shading represents the optimal maximum time shift


| 5 Year Shift |  | 10 Year Shift |  | 15 Year Shift |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a1 | 0.13585 | a1 | 0.25687 | a1 | 0.25314 |
| a2 | 3.5 | a2 | 3.5 | a2 | 3.5 |
| a3 | 0.23914 | a3 | 0.1643 | a3 | 0.16362 |
| a4 | -1.5628 | a4 | -1.9666 | a4 | -2.8292 |
| Se/Sy | 0.43868 | Se/Sy | 0.40902 | Se/Sy | 0.40902 |
| R2 | 0.91546 | R2 | 0.92694 | R2 | 0.92694 |

Note: Green shading represents the optimal maximum time shift

